¹ Welcome – Thanks for joining us. ITRC's Internet-based Training Program

> LNAPL Characterization and Recoverability – Improved Analysis



Do you know where the LNAPL is and can you recover it?

Sponsored by: Interstate Technology and Regulatory Council (<u>www.itrcweb.org</u>) Hosted by: US EPA Clean Up Information Network (<u>www.cluin.org</u>)

Light non-aqueous phase liquids (LNAPLs) are organic liquids such as gasoline, diesel, and other petroleum hydrocarbon products that are immiscible with water and less dense than water. LNAPLs are important because they are present in the subsurface at thousands of remediation sites across the country, and are frequently the focus of assessment and remediation efforts. A sound LNAPL understanding is necessary to effectively characterize and assess LNAPL conditions and potential risks, as well as to evaluate potential remedial technologies or alternatives. Unfortunately, many environmental professionals have a faulty understanding of LNAPL conditions based on outdated paradigms.

The ITRC LNAPLs Team is providing Internet-based training to improve the general understanding of LNAPLs. Better understanding leads to better decision making. Additionally, this training provides a necessary technical foundation to foster effective use of the forthcoming ITRC LNAPLs Team Technical Regulatory Guidance Document: Evaluating LNAPL Remedial Technologies for Achieving Project Goals (to be published in 2009).

This training course is relevant for new and veteran regulators, environmental consultants, and technically-inclined site owners and public stakeholders. The training course is divided into two parts:

LNAPL Training Part 1: An Improved Understanding of LNAPL Behavior in the Subsurface - State of Science vs. State of Practice - Part 1 explains how LNAPLs behave in the subsurface and examines what controls their behavior. Part 1 also explains what LNAPL data can tell you about the LNAPL and site conditions. Relevant and practical examples are used to illustrate key concepts.

LNAPL Training Part 2: LNAPL Characterization and Recoverability – Improved Analysis - Do you know where the LNAPL is and can you recover it? Part 2 addresses LNAPL characterization and site conceptual model development as well as LNAPL recovery evaluation and remedial considerations. Specifically, Part 2 discusses key LNAPL and site data, when and why those data may be important, and how to get those data. Part 2 also discusses how to evaluate LNAPL recoverability.

LNAPL Training Part 3: Evaluating LNAPL Remedial Technologies for Achieving Project Goals - uses the LNAPL conceptual site model (LCSM) approach to identify the LNAPL concerns or risks and set proper LNAPL remedial objectives and technology-specific remediation goals and performance metrics. The training course also provides an overview of the LNAPL remedial technology selection framework. The framework uses a series of tools to screen the seventeen remedial technologies based on site and LNAPL conditions and other important factors.

ITRC (Interstate Technology and Regulatory Council) <u>www.itrcweb.org</u> Training Co-Sponsored by: US EPA Technology Innovation and Field Services Division (TIFSD) (<u>www.clu-in.org</u>) ITRC Training Program: training@itrcweb.org; Phone: 402-201-2419



Although I'm sure that some of you are familiar with these rules from previous CLU-IN events, let's run through them quickly for our new participants.

We have started the seminar with all phone lines muted to prevent background noise. Please keep your phone lines muted during the seminar to minimize disruption and background noise. During the question and answer break, press *6 to unmute your lines to ask a question (note: *6 to mute again). Also, please do NOT put this call on hold as this may bring unwanted background music over the lines and interrupt the seminar.

You should note that throughout the seminar, we will ask for your feedback. You do not need to wait for Q&A breaks to ask questions or provide comments using the ? icon. To submit comments/questions and report technical problems, please use the ? icon at the top of your screen. You can move forward/backward in the slides by using the single arrow buttons (left moves back 1 slide, right moves advances 1 slide). The double arrowed buttons will take you to 1st and last slides respectively. You may also advance to any slide using the numbered links that appear on the left side of your screen. The button with a house icon will take you back to main seminar page which displays our presentation overview, instructor bios, links to the slides and additional resources. Lastly, the button with a computer disc can be used to download and save today's presentation slides.



The Interstate Technology and Regulatory Council (ITRC) is a state-led coalition of regulators, industry experts, citizen stakeholders, academia and federal partners that work to achieve regulatory acceptance of environmental technologies and innovative approaches. ITRC consists of all 50 states (and Puerto Rico and the District of Columbia) that work to break down barriers and reduce compliance costs, making it easier to use new technologies and helping states maximize resources. ITRC brings together a diverse mix of environmental experts and stakeholders from both the public and private sectors to broaden and deepen technical knowledge and advance the regulatory acceptance of environmental technologies. Together, we're building the environmental community's ability to expedite quality decision making while protecting human health and the environment. With our network of organizations and individuals throughout the environmental community, ITRC is a unique catalyst for dialogue between regulators and the regulated community.

For a state to be a member of ITRC their environmental agency must designate a State Point of Contact. To find out who your State POC is check out the "contacts" section at www.itrcweb.org. Also, click on "membership" to learn how you can become a member of an ITRC Technical Team.

Disclaimer: This material was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof and no official endorsement should be inferred.

The information provided in documents, training curricula, and other print or electronic materials created by the Interstate Technology and Regulatory Council ("ITRC" and such materials are referred to as "ITRC Materials") is intended as a general reference to help regulators and others develop a consistent approach to their evaluation, regulatory approval, and deployment of environmental technologies. The information in ITRC Materials was formulated to be reliable and accurate. However, the information is provided "as is" and use of this information is at the users' own risk.



Pamela Trowbridge is a Licensed Professional Geologist with the Pennsylvania Department of Environmental Protection (PA DEP) in Harrisburg. She has worked for the PA DEP since 1993. She is experience in regulation, guidance, policy, and procedure development and is working on developing guidance and procedures for addressing separate phase liquids in soils and groundwater. She assists sites under development through the Brownfield Action Team, a process that expedites the permitting process and the Land Recycling cleanup process, and provides technical assistance and input to Departmental permits for these sites. Pamela conducts training seminars of basic program information in the Land Recycling Program to consultants and the regulated community and provides training to DEP staff on new procedures and technical issues. Pamela has been the co-leader for the ITRC LNAPL Team since the team formed in 2007. She earned a bachelor's degree in earth sciences from Pennsylvania State University in University Park, Pennsylvania in 1992 and is a Licensed Professional Geologist in Pennsylvania.

Derek Tomlinson PE, PEng, BCEE, has specialized experience since 1994 in development of strategies for managing sites with dense and light non-aqueous phase liquids (DNAPL and LNAPL) and vapor intrusion (VI) concerns. Derek works for Geosyntec Consultants in Blue Bell, Pennsylvania. He is an environmental engineer with graduate training in contaminant hydrogeology including the characterization and remediation of sites contaminated with chlorinated solvents and migration of vapors within the subsurface. Derek has worked at refineries, waste sites, and other industrial facilities under USEPA CERCLA and RCRA programs; state and regional programs in California, Connecticut, Delaware, Georgia, Maryland, Massachusetts, New Jersey, Ohio, Pennsylvania, Rhode Island, Texas, Virginia, and West Virginia; and internationally in Australia, Brazil, Canada, China, and France. Technical expertise includes the design, implementation, and operation of a range of in situ remediation technologies within both porous media and fractured bedrock geologic settings. He was active with the ITRC LNAPL team and a contributing author for the LNAPL technical guidance and training documents. He is also active with ASTM and is contributing member that developed standard guides for LNAPL conceptual site models, LNAPL transmissivity calculation methods, and vapor intrusion assessments and mitigation strategies for real estate transactions. Derek earned a Bachelor degree in Civil Engineering in 1994 and a Master degree in 1999, both from the University of Waterloo in Waterloo, Ontario, Canada. He is a professional engineer in Pennsylvania and Canada and a Board Certified Environmental Engineer (BCEE).

Steven Ueland is a Principal with Langan Engineering and Environmental Services, Inc. in Doylestown, Pennsylvania. He started working for Langan in 1993. Steven is a professional engineer with over twenty two years of experience focusing on contaminated property characterization for the design and implementation of remediation/closure projects. His expertise includes hyrdogeologic assessment and strategic remedial planning for both Light and Dense Non-Aqueous Phase Liquid (NAPL) contamination sites. Steven's project experience has involved superfund site RI/FS, remedial design and construction oversight, UST closure/remediation, and NAPL assessment, mobility analysis and recovery system design for a large petroleum refinery. He served for two years on the U.S. EPA Region I Technical Assistance Team, where he had direct involvement in emergency response and hazard assessment and clean-up activities for oil spill incidents throughout New England. Steven also has expertise with oil spill contingency planning and regulatory compliance. Steven is currently responsible for a team of scientists and engineers addressing remediation and compliance for private industrial manufacturing sites. Steven is an active presenter at conferences, and has been a member of the ITRC LNAPLs team since its inception in 2007. Steven earned his bachelor's degree in civil engineering from the University of Vermont in Burlington, Vermont in 1986, and is a registered professional engineer in Pennsylvania and New Hampshire.







- In Part 1 of our training "Understanding LNAPL Behavior" or "LNAPL Basics," we discussed some common misconceptions about LNAPL behavior in the subsurface.
- LNAPLs do not float on the capillary fringe or groundwater table in a uniform, highly-saturated, "pancakelike" layer, as shown on the right. Instead, LNAPLs are distributed above, at, and below the groundwater table at saturations that vary vertically and horizontally in the soil, as shown on the left.
- As shown on the left, LNAPL saturations are not uniform. They are controlled by product type, soil type, and soil heterogeneity. LNAPL and water coexist in the soil pore space in the saturated zone. LNAPL, water, and air coexist in the soil pore space in the vadose zone.
- For a given apparent LNAPL thickness in a monitor well, the volume of <u>recoverable</u> LNAPL is usually
 greater from a coarse-grained soil (gravel & sand) than from a fine-grained soil (silt & clay). Thinking about
 it in another way, in an area of uniformly distributed LNAPL volume, the areas with the greatest apparent
 thicknesses in monitor wells usually correspond to the finest-grained (lowest permeability) soils. Because
 of the large apparent LNAPL thicknesses, these areas are commonly targeted for placement of free
 product recovery wells. However, large apparent LNAPL thicknesses in monitor wells in fine-grained soils
 do not necessarily mean that you will be able to recover significant volumes of LNAPL.
- As LNAPL saturations increase, such as during the release, the potential for LNAPL to migrate horizontally increases. Conversely, as the LNAPL saturation decreases it is less mobile and more difficult to recover.
- Why do we care about all this?
- Because use of the "pancake" model not only leads to overestimates of the total volume of LNAPL in the subsurface, but more importantly, it leads to overestimates of the recoverable volume of LNAPL in the subsurface.
- An estimation of the volume of recoverable LNAPL in the subsurface is necessary to determine when you can turn off your remediation system.
- "Recoverable LNAPL" can also be defined by the soil type and remediation method used to recover it. For example, skimmers can effectively remove free product from coarse-grained soils, but fine-grained soils may require vacuum-enhanced recovery systems.



•In order for LNAPL to migrate horizontally, the LNAPL must overcome the soil pore entry pressure in the saturated zone and capillary fringe soils.

•As shown in the picture, movement of the LNAPL "blob" is impeded by smaller water-wet soil pores.

•A measurable thickness of LNAPL in a monitor well does not necessarily indicate that the LNAPL is migrating. In fact, most LNAPL plumes come to stable configurations shortly after the release is stopped.

•Part 1 of this training discussed the basic principles for LNAPL distribution and mobility.

•This part of the training will focus on LNAPL characterization, the LNAPL Conceptual Site Model, and evaluation of LNAPL recovery.



•The purpose of today's training is to:

•Discuss LNAPL site characterization.

•Demonstrate how the concepts presented in the Part 1 training can be used to evaluate LNAPL recoverability.

•Discuss matching remedial technologies with remedial goals.



•This slide shows a cross-section of a typical LNAPL body, dissolved plume, and vapor cloud.

•The slide is from a publication by G.D. Beckett (Aqui-Ver) and David Huntley (San Diego State University). Beckett and Huntley have published many papers on LNAPL behavior in the subsurface and practical limits of LNAPL recovery.

•An LNAPL, such as gasoline, has leaked from an underground storage tank.

•The LNAPL has migrated down through the vadose zone soils to the groundwater table.

•The initial LNAPL release was large enough to create a smear zone below the water table. Historical water table fluctuations can also create smear zones below current water tables.

•The LNAPL body has moved out horizontally, radially - both upgradient and downgradient, in response to the initial LNAPL head or gradient. After the release is stopped, the LNAPL head dissipates and further expansion of the LNAPL body stops.

•The LNAPL body is still a source of contamination in the dissolved phase in groundwater and the vapor phase in the vadose zone soil gas.



•This slide shows three LNAPL conditions and associated remedial drivers.

•Panel 1 shows a condition where the LNAPL body is still migrating due to LNAPL head and high LNAPL saturations in the soil. LNAPL can migrate horizontally if the soils are saturated with LNAPL and there is an LNAPL head driving force. This condition is present during the initial LNAPL release. The remedial driver is LNAPL saturation. Removal of LNAPL will decrease the LNAPL head and stop further migration.

•Panel 2 shows a condition somewhat later where there is LNAPL present in monitor wells, but the LNAPL is no longer migrating. This is the condition at which we find most of our LNAPL sites. LNAPL in the soil near the release is at high saturations, but there is no longer an LNAPL head driving force, so the LNAPL body is stable. The LNAPL remedial drivers are LNAPL saturation and composition. Removal of LNAPL will shorten the life of the dissolved and vapor plumes. Removal of the more volatile/soluble/toxic <u>components</u> of the LNAPL (such as benzene) can mitigate explosion hazard risks, vapor intrusion hazard risks, and dissolved BTEX hazard risks.

•Panel 3 shows a condition where there is no longer LNAPL present in monitor wells. The LNAPL in soil is at saturations less than "residual saturation." "Residual saturation" is LNAPL that is left in the soil after all "free-draining" LNAPL has drained out. The remedial driver at this condition is LNAPL composition.

•This training will focus on Panels 1 and 2.



•This slide shows LNAPL concerns and remedial drivers.

•Removal of the more volatile/soluble/toxic <u>components</u> of the LNAPL (changing the LNAPL composition) will mitigate the LNAPL concerns shown on the left.

•Reducing the LNAPL saturation and LNAPL head will reduce the LNAPL mobility concern, which is mandated by EPA Regulation 40 CFR 280.64. This regulation states: "Remove free product to the maximum extent practicable, conduct free product removal in a manner that minimizes the spread of contamination into previously uncontaminated zones, and stop free product migration." This regulation further states: "Use abatement of free product migration as a minimum objective for the design of a free product removal system."

•Some States interpret this regulation to mean "remove free product to a 1/8 inch thickness in monitor wells," or "remove free product to a sheen" or "remove all free product."

•As we have discussed, removal of free product to these levels may not be possible or "practicable" depending on soil type and product type.

•In the 1996 EPA document: "How to Effectively Recover Free Product at Leaking Underground Storage Tank Sites" (EPA 510-R-96-001), the EPA stated that even under ideal conditions, engineered free product recovery systems will leave a significant proportion of LNAPL in the subsurface as an immobile residue.

•The purposes of this training are to educate consultants and regulators as to what is "practicable" when it comes to free product recovery and how to select a remediation technology based on the LNAPL concerns and drivers.



•The key to effective LNAPL management is development of a good LNAPL Conceptual Site Model.

•The basis of a good LNAPL Conceptual Site Model is a good LNAPL site characterization.

•A good LNAPL site characterization will include information on:

- the horizontal and vertical extent of the LNAPL body, dissolved plume, and vapor plume,
 potential receptors in the area, such as drinking water wells, subsurface utilities, and buildings overlying the plume,
- •the LNAPL product type (gasoline, diesel, or oil) and composition (fresh gasoline or weathered gasoline),

•soil types in the vadose zone and saturated zone,

•other data, such as pilot tests, that are necessary to evaluate remedial options.

•A good LNAPL Conceptual Site Model will use all the information from the LNAPL site characterization and pilot testing to develop an LNAPL management strategy.

•LNAPL management is an iterative process that includes refining the LNAPL conceptual site model and remedial action as new data is collected.



•Introduce Derek Tomlinson.



What is an LCSM?

A description and interpretation of the physical and chemical state of the LNAPL body and is the site characterization and management link.

Why is an LCSM of value?

Facilitates understanding of the LNAPL conditions, site risks, and how best to remediate.

When is an LCSM adequate?

When the LCSM provides quality of understanding of the LNAPL body and site risks to support necessary decision making and additional information likely would not lead to a different decision. This is an iterative process.

Level of effort?

Scaled to the LNAPL impacts and associated issues that require management



What does a LCSM cover?

Delineation (horizontal and vertical) – general geometry Age and Chemical/Physical Character Volume Mobility (or stability) – i.e. fluxes Longevity Recoverability Source / Pathway / Receptors



Ultimately want to understand the sources, pathways and receptors. As shown here we see a release of an underground storage tank and resulting LNAPL body. We have receptors and the risks associated with the LNAPL body could potentially pose emergency concerns such as utility corridors shown as 1, dissolved phase plumes impacting a drinking water well shown as 2, vapor concerns from both the LNAPL body and dissolved phase plumes shown as 3a and 3b, respectively. Other LNAPL risks associated with the LNAPL is the potential mobility from LNAPL within the LNAPL body or observed in wells shown as 4 and 5.

To provide the best management options for the given site, the professional should consider these components.



The complexity and amount of detail necessary within the LCSM increase with the increased complexity of the hydrogeologic and plume conditions and the concern related to potential risks. Simply put the more complex the site conditions are to understand, and the more concern there are with sensitive receptors and other risks, there is more value on a very good LCSM to make the best management decision.

An example of this is shown here graphically from ASTM LSCM guide. But basically put the complexity and level of detail in the LCSM follows can fallow a tiered approach. Developing a weight-of evidence determination for the level of complexity needed in the LCSM.

Factors that affect the complexity are shown in the above figure and in the ASTM guide:

•ASTM E2531 - Standard Guide for Development of Conceptual Site Models and Remediation Strategies for Light Nonaqueous-Phase Liquids Released to the Subsurface. Available from www.astm.org



No associated notes.





- Existing data
- Direct methods/conventional assessment
- Indirect methods
- Laboratory methods
- Database/empirical values

Remember: Not all of these data may be necessary

- Typically, when one is building the LCSM we are looking at existing data, as well as collection of new data. This data could be as simple as soil borings, groundwater and other direct / conventional methods, laboratory chemical and physical parameters, as well as other more innovative or "indirect" methods as well. Additionally, there are databases¹ and empirical values for sites available for the professional based on similar site soil types as well.
- 1. API Light Non-Aqueous Phase Liquid (LNAPL) Parameters Database and Guide for Data Retrieval (see www.api.org/Inapl)



From ASTM E2531.

These are some example LNAPL indicators but by no means is this an exhaustive list and not all of these indicators need to be assessed at a given site. Some example indicators are:

- 1. Known LNAPL release
- 2. Observed LNAPL (for example, in wells or other discharges)
- 3. Visible LNAPL or other direct indicator in samples
- 4. Fluorescence response in LNAPL range
- 5. Near effective solubility or volatility limits in dissolved or vapor phases
- 6. Dissolved plume persistence and center-of mass stability
- 7. TPH concentrations in soil or groundwater indicative of LNAPL presence
- 8. Organic vapor analyzer (OVA) and other field observations
- 9. Field screening tests positive (for example, paint filter test, dye test, shake test)



•Estimates of the source area can be based on observations in wells, boring logs, and other visual observations

•Uncorrected observations should not be used to estimate the volume or recoverability

•[CASE EXAMPLE] – site by river, top figure is a plot of observed LNAPL thicknesses in wells (i.e., apparent thickness). If one were to use these values/observations one would conclude that the LNAPL "upgradient" is connected to the River. However, as shown in the bottom image, the corrected using API models, observations of LNAPL vertical distributions with some innovative methods, and fingerprinting to discern LNAPL types, the picture is quite different and the LNAPL near the river is of immediate concern and the "upgradient" LNAPL self-contained

•As presented in Part 1, Seasonal fluctuations should be accounted into this assessment

•Locations of seeps along banks or other vertical cuts aid in characterizing LNAPL impacts to surface water bodies \leftarrow as shown in the example above.



Existing soil data is typically readily available for most sites. However, most of this more historic data is typically in the for of total petroleum hydrocarbon (TPH) data. One way to estimate what the potential saturation of LNAPL within the subsurface is use of an equation developed by Parker, Waddill and Johnson in 1994, which was also presented in the Natural Attenuation text by Wiedemeier, Rifai, Newell and Wilson in 1999.

Typically, information exists from the logs as well but may not necessary be to the detail one would like for a LNAPL assessment.

•Parker, J.C., Waddill, D.W., and Johnson, J.A., 1994. UST Corrective Action Technologies: Engineering Design of Free Product Recovery Systems, prepared for Superfund Technology Demonstration Division, Risk Reduction Engineering Laboratory, Edison, NJ, Environmental Systems & Technologies, Inc., Blacksburg, VA, 77 pp.

•Wiedemeier, T.H., H.S. Rifai, C.J.Newell, and J.T.Wilson, 1999. Natural Attenuation of Fuels and Chlorinated Solvents in the Subsurface. John Wiley & Sons, Inc., New York, NY, 617 pages. Equation on Page 77, equation 2.23.



No associated notes.



LNAPL thickness data over time

•LNAPL saturation limits and vertical extent

•Characteristics of the source zone, growing as shown in the early times form the Part 1 example

•Lateral stability of LNAPL body, becoming stable as shown in the example.

•Confined or unconfined conditions

•as will be discussed in the Recoverability example later in this presentation.



Key is detail, detail, detail. Can not have enough detail in logs within the core of the LNAPL body. An example of the detail is shown in this log noting lithology, water content, odor, soil structure, OVA readings and other subtle details. This is aided by use of shaker dyes (shown at bottom) and florescent lighting via a black box in the field or laboratory methods discussed later in this presentation. But what is evident is the variability in the saturation of the LNAPL qualitatively in the UV light image on the right. Shown on the left of this image is a white light photo of the soil, where one can see a zone of a sand lens near the top, which corresponds to a high observation of UV light in the core. LNAPLs tend to fluoresce due to the double bonds, the higher the fluorescence response; typically the more LNAPL is present.

Source of shaker image from: http://www.cheiron-resources.com; however, other vendors are available.



As noted, only molecules containing double bonds in the LNAPL phase will fluoresce. But we can use this to aid in understanding where is the LNAPL and qualitatively "how much" is there in the subsurface. Shown on the left is a typical LIF response output. In this example we see a perched zone in orange and a the typical response near the watertable with what we like to call the "shark fin". Along the left of the figure is the waveform, and this can be used to aid in discerning different LNAPL types if they have been properly tuned/calibrated by the operator. An example of an output that can be generated is zone in the middle center image. A image of the tool is zone on right and this is typically paired with a CPT point at the based of the probe.

More information available at: http://www.clu-in.org/char/technologies/lif.cfm



Membrane interface probe (MIP) is a semi-quantitative, field-screening device that can detect volatile organic compounds (VOC) in soil and sediment. Useful for identifying potential source zones in vadose zone. The negative of the tool with respect to LNAPL delineation is that is does not discern between sorbed phase, dissolved phase, or LNAPL.

Shown above is how the probe operates via a heating element that volatilizes the near membrane contaminants, a carrier gas within the probe (typically nitrogen) brings the VOCs to the GC/FID or GC/PID and other probes for measure (shown on bottom right). The probe is advanced via direct push (see top right) and the flights are strong with the gas tubing shown in the top center image.

More information is available at: http://cluin.org/char/technologies/mip.cfm



No associated notes.



Laboratory Analysis used to enhance LCSM

Soil, groundwater and vapor concentrations

Basic soil properties (e.g., grain size, bulk density, distribution, moisture content)

Specialized lab analysis packages have been developed to support LNAPL evaluations, primarily for modeling of LNAPL volumes and recoverability

Fluid properties

Pore fluid saturations and soil properties

Soil capillary properties (e.g., estimate van Genuchten / Brooks-Corey soil parameters)

Residual saturation

Fingerprinting

Specialized soil sampling and handling procedures

³¹ Specialized Laboratory Packages for LNAPL Characterization



| | What | When and Why |
|--|--|---|
| Fluids Properties Package - LNAPL and Water Pair | Dynamic viscosity and fluid density at three temps, surface and interfacial tension for each fluid pair (LNAPL/water, LNAPL/air, and air/water). ρ_o, μ_o, ρ_w, μ_w, σ_{ao}, σ_{ow}, σ_{aw} | Used for LNAPL recoverability evaluation Empirical data exists and can be used as an estimate Consider lab tests for unusual LNAPLs, LNAPL mixtures |
| Pore Fluid Saturation Package | Pore fluid saturations (NAPL and water) by Dean-Stark extraction; total porosity, air- filled porosity, grain density, dry bulk density, and moisture content. S_o, S_w, S_t, Φ | Used for LNAPL recoverability evaluation Pre and post-treatment testing to evaluate remedy effectiveness |

There are labs that have standardized packages, and with these parameters the professional can use sophisticated models and calculations to better understand the potential recoverability, and what parameters need to be manipulated by the remediation technologies to enhance the physical and chemical parameters to meet the site's management objectives. For instance, surface tension and viscosity can be manipulated via heating of the subsurface, or through the use of surfactants. The benzene or composition within the gasoline could be removed via air sparging or other like stripping technologies as an example.

Fluid Properties Package:

•ρ_o = specific gravity of oil [typical units g/cm³]

•µo = dynamic viscosity of oil [typical units cenitpoise, centistokes, Pascal-second]

• ρ_w = specific gravity of water [typical units g/cm³]

• μ_w = dynamic viscosity of oil [typical units cenitpoise, centistokes, Pascal-second]

 σ_{ao} = surface tension of oil (i.e., interfacial tension of air and oil) [typical units dynes/cm]

 $\bullet\sigma_{\sf ow}$ = interfacial tension of oil and water [typical units dynes/cm]

 $\bullet \sigma_{aw}$ = surface tension of water (i.e., interfacial tension of air and water) [typical units dynes/cm] Pore Fluid Saturation Package

•S_o = oil saturation within pore space [%] or normalized to scale of 1.0 of pore space

 $\circ S_w$ = water saturation within pore space [%] or normalized to scale of 1.0 of pore space

•S_t = total saturation

•Φ = total porosity (measure of void space within total volume) [dimensionless]

- •bulk soil density [typical units g/cm³]
- •soil grain density [typical units g/cm³]

Details about test methods are available in these notes and from API 4711 and API 4760, at www.api.org/Inapl, we unfortunately do not have the time in this training to go into the details of the methods; however, future trainings are planned to cover this topic in greater detail, as well as the upcoming technical guidance document.

Methods for Determining Inputs to Environmental Petroleum Hydrocarbon Mobility and Recovery Models, API Publication 4711, July 2001

LNAPL Distribution and Recovery Model (LDRM), API Publication 4760, January 2007

² Specialized Laboratory Packages for LNAPL Characterization (continued)



| | What | When and Why |
|---|--|---|
| Capillarity Package: Air/Water Drainage | Air/Water Drainage Capillary Pressure Curve (air displacing water) with Air Permeability and Hydraulic Conductivity: includes fluid production vs. capillary pressure, total porosity, dry bulk density. S_{wr}, Φ, K_w, (M, α), (λ, P_d) | Used for LNAPL recoverability evaluation Provides data needed to estimate van Genuchten, and Brooks-Corey water retention curve (calculated from data) |
| LNAPL Residual Saturation | Centrifuge and/or water drive S_{or} | Used for LNAPL recoverability evaluation Define effectiveness limits of dual and multi- phase extraction |

Capillarity Package: Air/Water Drainage

- •Swr = Irreducible water saturation
- •Φ = porosity

•K_w = hydraulic conductivity of water

•Water retention curve models

•Van Genuchten soil parameters:

•M = van Genuchten fitting parameter [dimensionless]

• α = van Genuchten fitting parameter [L²/F]

•Brooks-Corey soil parameters: λ , P_d

- •λ = lambda [dimensionless]
- $\cdot P_d$ = displacement pressure [F/L²]

LNAPL Residual Saturation

•S_{or} = Irreducible oil saturation

van Genuchten References:

van Genuchten, M. Th. (1980), "A Closed-form Equation for Predicting the Hydraulic Conductivity of Unsaturated Soils." Soil Science Society of America, No. 44, pp. 892-898.

van Genuchten, M. Th., F. J. Leij, and S. R. Yates. (1991), The RETC Code for Quantifying the Hydraulic Functions of Unsaturated Soils, Version 1.0. EPA Report 600/2-91/065, U.S. Salinity Laboratory, USDA, ARS, Riverside, CA.

Brooks-Corey References:

Brooks, R. H. and A.T. Corey (1966), "Properties of Porous Media Affecting Fluid Flow," Journal of the Irrigation and Drainage Division of the American Society of Civil Engineers, 4855 IR 2, June, pp. 61-88.

Brooks, R. H. and A.T. Corey (1964), Hydraulic Properties of Porous Media, Hydrology Paper Number 3, Civil Engineering Department, Colorado State University, Fort Collins, Colorado.

Corey, A.T. and R.H. Brooks, (1999), The Brooks-Corey Relationship, In Characterization and Measurement of the Hydraulic Properties of Unsaturated Porous Media, M.Th. van Genuchten, F.J. Leji, and L. Wu, Editors, University of California, Riverside, California, pp. 13-18. Corey, A.T. (1986), Mechanics of Immicible Fluids in Porous Media, Water Resources Publications, Littleton, Colorado.

Corey, A.T., C.H. Rathjens, J.H. Hemderson, and M.R.J. Wyllie (1956), "Three-Phase Relative Permeability," Journal of Petroleum Technology, Petroleum Transactions, AIME, November, pp.349-351.

<u>Comparing/Converting Between Both Models</u> Lenhard, R. J., J. C. Parker, and S. Mishra, 1989. On the Correspondence Between Brooks-Corey and Van Genuchten Models. <u>Journal of Irrigation and Drainage Engineering</u>, Vol. 115, No. 4, July/August 1989, pp. 744-751 Additional information regarding parameters:

Methods for Determining Inputs to Environmental Petroleum Hydrocarbon Mobility and Recovery Models, API Publication 4711, July 2001

LNAPL Distribution and Recovery Model (LDRM), API Publication 4760, January 2007



Define data needs based on assessment objectives

Laboratory packages may not include everything required and may include data not required

LNAPL parameters may be estimated

Published "default" or "average" parameters published for soil textural class determined from lithology and grain size distribution (e.g., API Interactive LNAPL Guide)

Empirical databases useful through comparison of basic site soil properties (e.g., grain size, bulk density)

(e.g., API Parameter Database)

Shown on this figure is an example of a Grain Size distribution (left), and a water retention curve (right)

References at www.api.org/Inapl:

 •LNAPL Distribution and Recovery Model (LDRM) API Publication 4760 January 2007
 •API Interactive LNAPL Guide Version 2.0

August 2004



No associated notes.



No associated notes.



As was mentioned earlier, the LCSM is a site characterization and management link. Ultimately a good LCSM will support the identification of appropriate objectives and setting relevant goals for the site, which will aid in the management options for the site.


Building on the concepts presented in the Part 1 training, this section will continue to build out the LNAPL Conceptual Site Model with the hydraulic recovery evaluation



Building on the concepts presented in the Part 1 training, this section will continue to build out the LNAPL Conceptual Site Model with the hydraulic recovery evaluation



Focus of talk and the hydraulic recovery evaluation is on the LNAPL body itself – represented here by numbers 4 and 5.

Both of these address the non-risk-based concerns of potential mobility and the aesthetic or regulatory concerns of LNAPL presence in a well.

Primary concern of both regulators and stakeholders....is the LNAPL moving?

Also represents one of the biggest misperceptions, that if there is LNAPL in a well, it is mobile and migrating and similarly recoverable.

Recoverability evaluation very important step in getting all parties on the same page with respect to understanding the LNAPL body and how to approach its remediation.



So how much LNAPL is potentially recoverable?

Illustrate this using the theoretical saturation profile.

The potentially mobile and therefore recoverable LNAPL is that amount that exists above the residual saturation.

Residual saturation is illustrated as two values - for both above and below the water saturated zone.

Why Do We Need to Evaluate LNAPL Recoverability for LCSM



- Determine site wide recoverability distribution
 - · Can interpolate Tn values to generate isopleths
- Determine if LNAPL can be recovered
 - In meaningful quantities
 - Sustained
- Determine where LNAPL can be recovered
- Assist with LNAPL recovery system management
 - Seasonal fluctuation may dictate that you only recover in certain period for example
- Determine when LNAPL recovery is complete

The objectives of recovery predictions are to design efficient free product recovery systems using trenches, skimmer wells and single and dual-pump wells, to provide estimates of recovery performance, to provide estimates of recovery time, and to provide a means of establishing practical endpoints. Over the next few slides, recovery predictions using analytical models will be described, so the relationship between the soil and fluid properties and the understanding developed earlier becomes clear.

Based on the complexities of LNAPL occurrence and behavior, and the misconceptions, LNAPL volumes and recovery are typically over-estimated.

Important point to remember, however, is that LNAPL recovery is limited and finite. As you recover the LNAPL, its saturation is being decreased, and therefore, its mobility and recoverability is diminishing.



Several ways to assess recoverability



The weight of evidence approach can be very useful for evaluating mobility.

This topic is discussed in relatively new documents from the Massachusetts Licensed Site Professionals, as well as a recent guidance document from the Wisconsin Department of Commerce and Natural Resources.

Wisconsin Department of Commerce & Wisconsin Department of Natural Resources Assessment Guidance for Sites with Residual Weathered Product (PUB-RR-787):

http://prodoasext.dnr.wi.gov/inter1/pk_rr_doc_public\$doc.QueryViewByKey?P_DOCUMENT_SEQ_N O=8990&Z_CHK=8923.

Massachusetts Licensed Site Professionals LNAPLs and the Massachusetts Contingency Plan Part I:

http://www.mass.gov/dep/cleanup/lnaplwg.htm

Massachusetts Licensed Site Professionals LNAPLs and the Massachusetts Contingency Plan Part II:

http://www.mass.gov/dep/cleanup/Inaplwg.htm

A spill of heavier oil such as No. 6 fuel is a simple example, where we know that this material is not mobile under typical subsurface temperatures.

A known release date or volume are also very useful indicators for potential recoverability, as it is generally well understood that LNAPL spills spread out relatively quickly, and reach of point of stability within a short period of time.

Plume stability can demonstrated fairly easily using historic monitoring data that has been collected consistently over time.



An LNAPL baildown test is performed and analyzed very similarly to a water baildown test but with some important differences. First, instead of the water being evacuated from the well, only the LNAPL is removed – in practice this is hard to do. We often try to do it with a vacuum truck rather than a bailer. Instead of only monitoring the water-air interface, both the water-LNAPL and LNAPL-air interfaces need to be monitored versus time. The figure shows a plot of such data.

There are two methods for analyzing the data. The first is that of Lundy and Zimmerman, and the second is that of Huntley. We typically use both and compare them to theory.

There are practical limitations to the test. First, there needs to be enough LNAPL in the well to measure and determine a change in thickness of LNAPL flow into the well. Second, the conductivity of the LNAPL needs to be great enough that the LNAPL flows back into the well. Thus, for high viscosity liquids (about 10 centipoise or higher) or low permeability soils, several days may be required for the LNAPL to flow into the well which could be a problem if the potentiometric surface also changes.

Similar to a typical slug test for determining soil hydraulic properties

Baildown test involves rapidly removing LNAPL from the well while minimizing recovery or disturbance of the groundwater.

Although this is a short term test and quite simple, it can provide valuable information.



The baildown test can then be used to calculate the oil transmissivity.

This solution has been described by David Huntley at San Diego State University.

The calculation of T from baildown tests is based on modifications of the familiar slug test solutions provided by Bower and Rice and Cooper-Jacobs, correcting for LNAPL fluid properties and multiple fluid phases in the system.

Very useful way to quantify LNAPL mobility.

Reference: A Protocol for Performing Field Tasks and Follow-up Analytical Evaluation for LNAPL Transmissivity Using Well Baildown Procedures, G.D. Beckett, AQUI-VER, Inc. and M.A. Lyverse, Chevron Texaco Energy Research and Technology Co., August 2002.



Pilot tests provide some of the most valuable information regarding potential LNAPL recoverability, particularly for simpler sites where more complex modeling may not be warranted.

Similar to baildown tests, they can be used to quantify important parameters such as T.

Slide shows real data from a site with multiple varying product bodies over a fairly large area.

The bar chart summarizes the total volume of LNAPL recovered from each of several wells over a 48-hour skimming pilot test conducted in each well.

Total recovered volumes ranged from less than 10 gallons to over 250 gallons.

It must be noted that the total recovered volumes from the wells does not correlate with the initial product thickness in the wells



The graphic at the right shows both a soil core and a monitoring well under ultraviolet light.

The LNAPL conditions in the soil and well fluoresce.

The typical LNAPL saturation profile illustrates saturation over the vertical interval.

Highest LNAPL saturation has highest conductivity.

Low saturation = low conductivity

Hydraulic recovery is proportional to T, and is not indicated accurately by LNAPL well thickness



These next two slides provide an example using real site data.

Baildown test, but only shows recovered (rebounded) LNAPL thickness.

This first graph illustrates the results of baildown tests on three wells, each with a different initial LNAPL thickness.

These test results were used to calculate transmissivity for each well.

⁴⁹ LNAPL Transmissivities and Thicknesses (in a Well)



| | Approximate | Recovery Rate B Test | | |
|-----------|-----------------------------|-------------------------|---|---|
| Location | Gauged Thickness (ff) | LNAPL Skimming (GPD) | 1 GPM - Water Enhanced Recovery (GPD) | LNAPL Transmissivity (ff ² /day) |
| AMR/200-D | 15 | 40 | 115 | 4 |
| AMR/185-6 | 30 | 0.4 | 0.7 | 0.01 |
| AMR/606-D | 34 | 2 | 5.7 | 0.2 |

Key Points:

- ► LNAPL thickness is a poor indicator of LNAPL recoverability → thickness is too dependent on soil type, heterogeneity, water levels, LNAPL occurrence (confined, perched, unconfined), etc.
- Transmissivity (via baildown tests, pilot test, or existing recovery data) is a more direct measure of LNAPL recoverability that factors in soil type heterogeneity and water levels.

(Atlantic Richfield Corporation, 2008)

This slide shows a comparison of the data for the three wells tested on the previous slide.

This table provides transmissivity and recovery calculations for the wells on the previous slide. Note the well with the greatest LNAPL thickness (34 ft!) recovers much more slowly and has lower LNAPL recovery rates than the well with 15 ft of LNAPL thickness.

The well with the least thickness resulted in the best recovery rate; and the wells with much higher thicknesses resulted in much lower recovery.

The transmissivity values correlated well with the recovery rates.



The next several slides present desktop methods to assess recoverability.

The first slide presents the decline curve analysis. This is a great way to extrapolate existing system performance data to predict total recoverability.

For mature and efficient recovery systems operated in a consistent mode – the declining recovery data will fit a straight line.

Extrapolation of the straight line to some practical recovery rate provides an estimate of total recoverable LNAPL.



This slide provides a real life example.

The blue bars indicate daily recovery.

The cumulative recovery curve, shown in red, illustrates the typical asymptotic curve where continued system operation is having little benefit adding to the total cumulative recovery of approximately 3,700 gallons.



This slide is showing the same site data as the previous slide, plotted using the decline curve.

The best fit line through the data, extrapolated to the x-axis or zero recovery rate, indicates the total maximum recoverable volume.

In this case, the extrapolation is very short as the system had already reached its practical limit, again at a total recovery of around 3,700 gallons.



Links to these API resources are provided in the end of this training.

American Petroleum Institute Light Non-Aqueous Phase Liquid Resource Center:

<u>http://www.api.org/ehs/groundwater/Inapl/index.cfm</u>. The LNAPL Resource Center contains manuals, software and other technical material to help you address cleanup of free-phase petroleum hydrocarbons in the shallow subsurface.



It is important to remember the underlying assumptions behind these model solutions.

As you learned in the Part 1 training, these are typically based on the vertical equilibrium (VEQ) model and utilize in well LNAPL thickness for an unconfined aquifer.

These models are typically appropriate for more complex sites and can be very useful to predict and help assess different recovery scenarios.



Using single layer API model.

This slide shows an example of a good model prediction of actual system recovery.

During system operation, it was found that nearby pumping conditions by others were varying substantially and therefore, affected the accuracy of the model predictions.



Using LDRM 3-layer model.

This slide illustrates the results of updated site modeling performed using a three layer model and additional years of recovery.

As shown by the updated orange model prediction, the three layer model was more representative and better matched the actual recovery system performance.



The user must assess the uncertainty behind the modeled solutions.

Even when done very carefully, models should be considered approximations



Case 4 is the development of a recovery plan for LNAPL at a closed refinery that has reuse potential. It is a RCRA site of 250 acres underlain by LNAPL some of which has a very low conductivity and some of it is at residual saturation. There are about 180 acres of LNAPL that may have the potential to migrate.

The question was how to define "potential to migrate".

The Remedy Decision for the site is that LNAPL recovery is required when: LNAPL with the potential to migrate exists within 300 ft of downgradient boundary – the question is how to define "potential to migrate". This will be explored using our new understanding. The other Remedy Decision is when LNAPL is a source of benzene to groundwater; this will not be explored here because the subject is beyond this training.



This figure depicts the areas that were suspected of containing LNAPL that had an ability to migrate. The different colors (yellowish and pinkish) are from different investigations and don't mean anything for this training. The receptor is the North Platte River.

Figure shows the site area initially suspected of having LNAPL with the potential to migrate.



The analysis method used here was performed by Brubaker and others, and involved developing a corrected LNAPL saturation profile with depth by correlating saturation data from LIF/ROST, with saturation measurements from soil borings across the site.

This profile was then correlated with saturation curves calculated using the API spreadsheet. This data is shown in the figure on the left.

The saturation data was then used to make conductivity predictions vs. depth that were then validated with baildown tests.

The right figure shows the agreement that can be expected between calculated and baildown test-determined conductivities.

Scatter in data is due primarily to the varying distance between tested wells and the corresponding borings used for the calculated conductivities, however, overall the graph Illustrates reasonable predictions.



This map was generated to illustrate the distribution of LNAPL transmissivities calculated using the API spreadsheet.

Substantial area, approximately 179 acres, is represented by the low transmissivity values.



In regulatory negotiation and incorporating the potential reuse of the site, the LNAPL recovery was only to be implemented within areas that contain benzene impacted LNAPL at an initial conductivity greater than 10⁻⁴ cm²/sec. This corresponds to 0.15 ft thickness with a gasoline type product and is approximately 46 acres whereas approximately 180 acres were previously thought to require recovery. This saves a substantial amount of resources for other beneficial uses.





The other typical metric used is LNAPL recovery rate. Recovery rate is a more robust metric than apparent LNAPL thickness. However due to a number of variables such as operational issues, potential confining conditions, and fluctuating water tables, recovery systems typically exhibit variability with regards to LNAPL recovery. This point will be illustrated in the example we'll go over.

LNAPL thickness is a poor indicator for recoverability, and in fact can be quite misleading.

By comparison, LNAPL transmissivity as a remediation metric factors out these variables, resulting in a metric that is dependent primarily on the relative level of free-phase LNAPL impacts.



illustrated in this modeled example, our monitoring well post-hydraulic recovery is shown without any LNAPL thickness.

It must be noted that this is not always the case, and that well thicknesses can occur following a practical end point to hydraulic recovery.



Important to understand potential risks associated with residual LNAPL left behind following recovery.

As illustrated in the figure on the right, removal of all recoverable LNAPL does not reduce the dissolved benzene concentration.



Will mass recovery of LNAPL abate the risks and concerns associated with the LNAPL?

And what are the appropriate remediation objectives for LNAPL?



| ⁹ Objec Perfo | ctives, Goals an rmance Metrics | d | | | |
|-----------------------------|---|---|----------------------|--|--|
| Objective: | A remedial objective to abate each LNAPL concern. | | | | |
| Goal: | A remediation goal for each LNAPL remedial objective. | | | | |
| Performance Metric: | A performance metric for each | remediation goal. | | | |
| Examples | Scenario 1 | Scenario 2 | | | |
| Objective | Stop LNAPL migration off site. (Saturation Objective) | Stop dissolved BTEX plume in groundwater from migrating off site. (Composition Objective) | | | |
| Goal | Remove LNAPL by skimming to reduce LNAPL head and stop LNAPL migration. | Remove BTEX components in the LNAPL using air sparging & vapor extraction. | | | |
| Metric | No LNAPL appearing in monitor wells on property line. | BTEX less than MCLs in mo wells at downgradient prope | onitor erty line. | | |

•Now that we have characterized the site, developed an LNAPL conceptual site model, identified LNAPL concerns, and evaluated LNAPL recoverability, we need to establish remedial objectives, remediation goals, and performance metrics.

•For example:

- In Scenario 1, the LNAPL concern is LNAPL migrating off site. The remedial objective is to stop LNAPL migration. The remediation goal is to remove enough LNAPL using skimmers to reduce LNAPL head so that LNAPL migration is stopped. The performance metric is to have no LNAPL appear in monitor wells on the property line.
- In Scenario 2, the LNAPL concern is a dissolved BTEX plume migrating off site. The remedial objective is to stop the dissolved BTEX plume from migrating off site. The remediation goal is to remove the soluble and volatile components in the LNAPL to allow natural attenuation to abate the dissolved BTEX plume before it migrates off site. The performance metric is to have no dissolved BTEX detected in monitor wells on the downgradient property line.

•Establishing remedial objectives, remediation goals, and performance metrics up front is important. •Slide 72.





- ▶ Start with the end in mind
- Get stakeholders on the same page
- Get stakeholders to agree on what is realistically achievable
- Discuss remedial objectives and remediation goals
- Long-term vision may be revised if goals are later found <u>not</u> to be achievable
- EPA, March 2005, "A Decision-Making Framework for Cleanup of Sites Impacted with LNAPL" (EPA 542-R-04-011)






•As we have discussed, removal of all LNAPL may be impossible at some sites.

•According to the Wisconsin Department of Natural Resources, RE NEWS, December 2002, about a dozen sites with residual free product are closed by DNR each year.

•In San Diego, California, the Department of Environmental Health has closed three LUST sites with residual free product (1997, 2005, and 2009).







•As the illustration shows, the relative permeability of LNAPL in soil decreases as the LNAPL saturation decreases. In other words, as more LNAPL is removed, the ability to keep removing LNAPL decreases.



•Vapor extraction in combination with air sparging, in-situ heating (ERH), or steam injection removes the more volatile components from the LNAPL body.



•It takes an LNAPL head or gradient for LNAPL to overcome soil pore entry pressures and migrate horizontally.

•LNAPL skimming or pumping can create an LNAPL gradient and induce LNAPL flow to a recovery well. Hydraulic recovery methods change the hydraulic gradient of the groundwater which can indirectly increase the LNAPL gradient.

•Low viscosity fluids flow more readily than higher viscosity fluids. Heating the LNAPL can reduce LNAPL viscosity and enhance removal.

•LNAPL flow and recovery can be enhanced by lowering the interfacial tension and wetting contact angles between soil pore water and LNAPL. The LNAPL interfacial tension and wetting contact angles can be reduced by surfactants and co-solvents.





•In porous media, the smallest pores will adsorb water first and hold it the tightest.

•It takes significant pressure to get the water out of the smallest pores. This is why coarse sands and gravels have a relatively small capillary fringe, while silts and clay have a large capillary fringe (and hence, stay moist). Because of the smaller pore sizes, silts and clays hold LNAPL and water more tightly and exhibit a higher capillary pressure than sands.

•Surfactants and cosolvents reduce interfacial tension and allow residual LNAPL to be removed from small pores and flow to a recovery well.





•LNAPL remedial options can focus on the LNAPL source by removal, focus on the pathway by containment, or focus on the receptor by controlling exposure.

•As this slide shows, natural source zone depletion is already occurring at the LNAPL source and along the pathway. NSZD may prevent the contaminants from reaching a receptor, however, it must be evaluated carefully.

•The ITRC Technology Overview document: "Evaluating Natural Source Zone Depletion at Sites with LNAPL" dated April 2009 provides detailed guidance on how to evaluate NSZD.



•There are natural processes that begin when the LNAPL is released into the environment. These processes occur regardless of any remediation technology being applied.

•The ITRC LNAPL team developed a Technology Overview document that details NSZD and presents methods to quantify these LNAPL mass loss processes.

INTERSTATE 84 **LNAPL** Technical Regulatory **Guidance Document** 1. Excavation ITRC LNAPL Team Tech/Reg 2. Physical Containment Guidance facilitates the 3. In-situ Soil Mixing selection of appropriate Natural Source Zone Depletion (NSZD) 4. LNAPL remedial technologies: 5. Air Sparging/Soil Vapor Extraction LNAPL site conditions (AS/SVE) LNAPL properties 6. LNAPL Skimming LNAPL remedial objective • 7. Bioslurping/Enhanced Fluid Recovery LNAPL remediation goals 8. Dual Pump Liquid Extraction (DPLE) (tech specific) 9. Multiphase Extraction (Dual Pump) LNAPL performance 10. Multiphase Extraction (Single Pump) metrics (tech specific) 11. Water Flooding Internet-based Tech-Reg 12. In-situ Chemical Oxidation Training in 2010 13. Surfactant-Enhanced Subsurface KEY POINT: Remediation (SESR) 14. Cosolvent Flushing Remediation technology 15. Steam/Hot-Air Injection selection criteria are 16. Radio Frequency Heating presented in the ITRC 17. Three and Six-Phase Electrical LNAPL Tech/Reg Guidance. Resistance Heating

•The ITRC Tech/Reg Guidance document facilitates the selection of appropriate remedial technologies based on site conditions and remediation goals.





Links to additional resources: http://www.clu-in.org/conf/itrc/LNAPLcr/resource.cfm

Your feedback is important – please fill out the form at: http://www.clu-in.org/conf/itrc/LNAPLcr/feedback.cfm

The benefits that ITRC offers to state regulators and technology developers, vendors, and consultants include:

✓ Helping regulators build their knowledge base and raise their confidence about new environmental technologies

✓ Helping regulators save time and money when evaluating environmental technologies

 \checkmark Guiding technology developers in the collection of performance data to satisfy the requirements of multiple states

 \checkmark Helping technology vendors avoid the time and expense of conducting duplicative and costly demonstrations

✓ Providing a reliable network among members of the environmental community to focus on innovative environmental technologies

How you can get involved with ITRC:

 \checkmark Join an ITRC Team – with just 10% of your time you can have a positive impact on the regulatory process and acceptance of innovative technologies and approaches

- \checkmark Sponsor ITRC's technical team and other activities
- ✓Use ITRC products and attend training courses
- ✓ Submit proposals for new technical teams and projects