



Most decisions at groundwater contamination sites are driven by measurements of contaminant concentration – snapshots of contaminant concentrations that may appear to be relatively stable or show notable changes over time. Decisions can be improved by considering mass flux and mass discharge. Mass flux and mass discharge quantify the source or plume strength at a given time and location resulting in better-informed management decisions regarding site prioritization or remedial design as well as lead to significant improvements in remediation efficiency and faster cleanup times. The use of mass flux and mass discharge is increasing and will accelerate as field methods improve and practitioners and regulators become familiar with its application, advantages, and limitations. The decision to collect and evaluate mass flux data is site-specific. It should consider the reliability of other available data, the uncertainty associated with mass flux measurements, the specific applications of the mass flux data, and the cost-benefit of collecting mass measurements.

The ITRC technology overview, Use and Measurement of Mass Flux and Mass Discharge (MASSFLUX-1, 2010), and associated Internet-based training provide a description of the underlying concepts, potential applications, description of methods for measuring and calculating, and case studies of the uses of mass flux and mass discharge. This Technology Overview, and associated Internet-based training are intended to foster the appropriate understanding and application of mass flux and mass discharge estimates, and provide examples of use and analysis. The document and training assumes the participant has a general understanding of hydrogeology, the movement of chemicals in porous media, remediation technologies, and the overall remedial process. Practitioners, regulators, and others working on groundwater sites should attend this training course to learn more about various methods and potential use of mass flux and mass discharge information.

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## 5 Meet the ITRC Trainers **Chuck Newell** Alex MacDonald **GSI Environmental Inc California Water Boards** Houston, TX Rancho Cordova, CA 713-522-6300 916-464-4625 cinewell@gsi-net.com amacdonald@ waterboards.ca.gov Alec Naugle Tamzen Macbeth **CDM Smith** Oakland, CA



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INTERSTATE

Alex MacDonald is a senior engineer in the technical support section of the Cleanup Unit at the Central Valley Regional Water Quality Control Board in Rancho Cordova, California. He has worked at the Water Quality Control Board since 1984. He primarily works on cleanup of the Aerojet site in Rancho Cordova, California and other nearby sites such as McClellan Air Force Base. Alex has also worked on cleanup at underground and above ground storage tanks sites; permitting and inspection of landfill and waste disposal to land sites; regulating application of biosolids sites; regulating NPDES sites that include wastewater treatment plants, power plants, industrial facilities, and groundwater treatment facilities; and permitting and inspecting dredging projects. Alex was a member of the ITRC Perchlorate team. Alex earned a bachelor's degree in Civil/Environmental Engineering from Stanford University in Palo Alto, California in 1977 and a master's degree in Civil/Environmental Engineering from Sacramento State University in Sacramento, California in 1987.

Dr. Tamzen Macbeth is a Vice President at CDM Smith out of Helena, Montana. She has worked for CDM since 2009. Previously, she worked for 7 years at North Wind Inc. Tamzen is an environmental engineer with an interdisciplinary academic and research background in microbiology and engineering. She specializes in the development, demonstration and application of innovative, cost-effective technologies for contaminated groundwater. Specifically, she is experienced in all aspects of remedies from characterization to remediation for DNAPLs, dissolved organic, inorganic, and radioactive contaminants under CERCLA and RCRA regulatory processes. She has expertise in a variety of chemical, biological, thermal, extraction and solidification/stabilization remediation techniques as well as natural attenuation. Her current work focuses developing combined technology approaches, and innovative characterization techniques such as mass flux and mass discharge metrics. Since 2004, Tamzen has contributed to the ITRC as a team member and instructor for the ITRC's Bioremediation of DNAPLs, Integrated DNAPL Site Strategy, Molecular Diagnostics and DNAPL Characterization teams. Tamzen earned a bachelor's degree in Microbiology in 2000 and a master's degree in Environmental Engineering in 2002 both from Idaho State University in Pocatello, Idaho, and a doctoral degree from in Civil and Environmental Engineering in 2008 from the University of Idaho in Moscow, Idaho.

Dr. Charles (Chuck) J. Newell, Ph.D., P.E. is a Vice President of GSI Environmental Inc in Houston, Texas and has worked for GSI since 1989. His professional expertise includes site characterization, groundwater modeling, non-aqueous phase liquids, risk assessment, natural attenuation, bioremediation, non-point source studies, software development, and long-term monitoring projects. He is a member of the American Academy of Environmental Engineers, a NGWA Certified Ground Water Professional, and an Adjunct Professor at Rice University. He has co-authored five U.S. EPA publications, eight environmental decision support software systems, numerous technical articles, and two books: Natural Attenuation of Fuels and Chlorinated Solvents and Ground Water Contamination: Transport and Remediation. He has taught graduate level groundwater courses at both the University of Houston and Rice University. He has been awarded the Hanson Excellence of Presentation Award by the American Association of Petroleum Geologists, the Outstanding Presentation Award by the American Institute of Chemical Engineers, and the 2001 Wesley W. Horner Award by the American Society of Civil Engineers (for the paper, "Modeling Natural Attenuation of Fuels with BIOPLUME III"). He was recently cited as the Outstanding Engineering Alumni from Rice University in 2008. He earned a bachelor's degree in Chemical Engineering in 1978, a master's degree in Environmental Engineering in 1981, and a Ph.D. in Environmental Engineering in 1989, all from Rice University in Houston Texas. Chuck is a professional engineer registered in Texas.

Alec Naugle, P.G. is a Senior Engineering Geologist in the Groundwater Protection Division at the California Regional Water Quality Control Board. San Francisco Bay Region where he has worked since 1999. Alec leads a unit that oversees solvent and petroleum hydrocarbon cleanups at Department of Energy laboratories and closed military bases, many of which are undergoing conversion for civilian use. He is also co-chair of the Region's technical groundwater committee, which supports the Board's planning activities related to groundwater guality and beneficial use. Prior to joining the Board, Alec worked as a consultant on various military and private sites in California and the Northeast and as a regulator in the UST program. Alec has been a member of ITRC since 2000 participating in the Permeable Reactive Barriers, Enhanced Attenuation: Chlorinated Organics, and Integrated DNAPL Site Strategy teams. Alec earned a bachelor's degree in chemistry and geology from Marietta College in Marietta, Ohio in 1986 and a master's degree in groundwater hydrology from the University of California at Davis in 2001. Alec is a Registered Professional Geologist in California.





ITRC's documents on DNAPLs are available from http://www.itrcweb.org/Guidance





I NPDES permits you are required to report concentration and mass measurements





Near the end of today's presentation we have several case studies that show how mass flux has been applied at several sites across the country to help remediate sites more efficiently. Pay attention to the presentation between now and then so you can see how to apply mass flux concepts that helped this site at Reese Air Force Base significantly address its groundwater contamination as shown by the shrinking plumes depicted here.



This section discusses the fundamental concepts of mass flux and discharge: the definitions, how these metrics compare to concentration data, how flux and discharge can be estimated, how flux and discharge change over time as sources and plumes evolve, and how flux and discharge can be valuable for site management.





Fundamental principles of contaminant hydrogeology. Terms are often confused – in particular, "mass flux" is often used for both concepts. Measures the total mass of contaminant, or other solute, in motion. Measuring mass flux identifies the variations in the mass and flow velocity across a plume.

Excellent fundamental descriptions are given in:

R. B. Bird, W. E. Stewart, and E. N. Lightfoot. Transport Phenomena. Revised 2<sup>nd</sup> ed., 2007. John Wiley & Sons, Inc.

C.W. Fetter. Contaminant Hydrogeology. 2<sup>nd</sup> ed., 1999. Waveland Press, Inc.



Transitioning into mass discharge—

Mass discharge is equivalent to source or plume strength. Looking down on a plume, a transect immediately down gradient of the source measures the mass loading to the plume, which changes with time, and transects further downgradient measure the mass in motion. The difference in mass discharge with distance is the natural attenuation rate, in a plume that is stable.









Both concentrations and groundwater velocity can vary dramatically over short distances. Both can also vary over time, seasonally and over longer time frames. The spatial variation in 3 dimensions is generally far more complex than typical representations of contaminant plumes suggest, and it can be important to understand these variations.



Illustrative example of an aquifer with identical concentrations and gradients in three sandy layers. But mass flux varies about 30-fold between layers, because the hydraulic conductivity varies, so that 85% of the flux is through only one layer. Even in unconsolidated aquifers, 80-90% of the mass flux may be through only 10-20% of the total plume volume.

Note that the groundwater and mass discharge are based on the Darcy velocity (Q=Ki) and not the seepage velocity (Vs=Ki/p), where p = porosity. The seepage velocity, which is the average fluid velocity within the pores, is faster than the Darcy velocity, which refers to the rate of movement of water through the entire area of a plane across the flow direction.





In the early phases, most of the mass is in the transmissive zones.

Later, mass diffuses into the lower-permeability zones.

Finally, plumes are sustained by back-diffusion, with relatively little flux in higher-K zones. Mass flux distribution indicates where to treat most mass and whether back-diffusion is a likely problem.



EPA, 2002 reference: EPA 542-R-02-008a-u, November 2002, Pilot Project to Optimize Superfund-financed Pump and Treat Systems: Summary Report and Lessons Learned. More information available at

http://www.epa.gov/tio/download/remed/rse/phase\_ii\_report.pdf

















## 32 How Many Points? Depends on Use Information from Table 1.1



Remedial Applications	Mass Flux Data Use	Relative Data Density Needeo
Active remediation or MNA	Estimate source strength	Low
	Estimate plume stability	High*
	Estimate mass balance-natural attenuation capacity	Medium to High
Evaluate risk to eceptor(s)	Estimate risks and exposures at various points of potential exposure	Low to Medium
Select appropriate technology	Determine remedial action objectives	Low to High
	Determine appropriate remedial technology(ies)	
Develop/optimize remedial design	Evaluate heterogeneities in source architecture	High
	Estimate source strength reductions necessary to transition technology (e.g., in situ biorem. or MNA)	Low
	Estimate distribution of contaminants	High
Evaluate remedial performance	Compare actual mass removal to design. Compare electron acceptors to electron donors	Low to High**
Evaluate compliance / LTM	Determine mass discharge or flux limits to achieve remedial goals	Low to Medium


































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fransverse				DISSOLVEI	HYDROCAR		CENTRATIO	NS IN PLUMI	(mg/L at Z=	0)		
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leasurement Method 5 lodels with Mass Discharge			
Model	Model application and type		
BIOSCREEN	Fuel Hydrocarbon MNA, Analytical		
BIOCHLOR	Chlorinated Solvent MNA, Analytical		
BIOBALANCE	Chlorinated Solvent MNA, Analytical		
MODFLOW/MT3DMS	General. Numerical		
MODFLOW/RT3DMS	General, Sequential Degradation, Numerical		
MODFLOW/MT3D	General. Numerical		
MODFLOW/RT3D - rtFlux	General. Numerical		
REMChlor New!	Hydrocarbon, Chlorinated Solvent		
	From Table		











•Based on review of case studies we identified five categories of mass flux and mass discharge "uses":

•Some categories, like "site characterization" and "remediation" are fairly broad and encompass several sub-categories

•And it should be noted that some sub-categories of "site characterization" may occur after a remedy has been selected, but there is reason to suspect things are working as planned due to incomplete site characterization, so the site characterization uses don't necessarily happen in the beginning.

- 1.Site Characterization
- 2.Potential Impact Assessment
- 3.Remediation
- 4.Compliance Monitoring
- 5.Site Prioritization





The use of Mass Flux and Mass Discharge is increasing, as the chart shows Includes all "use" categories:

- 1. Site Characterization
- 2. Potential Impact Assessment
- 3. Remediation
- 4. Compliance Monitoring
- 5. Site Prioritization







## <sup>63</sup> Mass Discharge Calculations for Various Sites



Site	Contaminant	Mass Discharge (g/d)	Reference	
Sampson County, NC	MTBE	0.6 - 2	(Borden et al, 1997)	
Vandenberg AFB, CA	MTBE	4 - 7	Unpublished	
Unnamed Site	MTBE	4	Unpublished	
Elizabeth City, NC	MTBE	7.6	Wilson, 2000	
St. Joseph, MI	TCE	167	(Semprini et al, 1995)	
Dover AFB, DE	CVOCs	630	(RTDF 1998)	





This figure illustrates why using mass flux and mass discharge can improve remedy selection, design, and performance monitoring.

In this case, there are 3 sandy layers each with identical gradients (.003). But conductivity varies among them 33-fold, from 1 m/day in the fine sand layer at the top to 33 m/day in the gravelly sand, and the concentrations vary by two orders of magnitude from 50 ug/L in the gravelly sand to 5,000 ug/L in the fine sand top layer. In this figure, the highest concentration is in the least permeable layer.

As a result, the mass flux is highest in the fine sand at 15 mg/day/m2 and lowest in the gravelly sand at 5 mg/day/m2.





I NPDES permits you are required to report concentration and mass measurements





So far we've heard very useful information about how mass flux and mass discharge can be used to support site characterization and remediation, and amount some of the interesting methods for estimating mass flux and mass discharge.

Even though the use of these mass data isn't new, the frequency of use of mass data has grown rapidly in the past few years. To gain some insights on how these data are being used across the industry, we conducted a detailed review of about 65 case studies where mass flux or discharge were estimated.

The results of this detailed review are included in tables in an appendix at the back of the Overview document, including a summary of site-specific mass discharge estimates with different methods, value added to the site through the use of mass, numbers and spaces between wells when used with the transect method, etc.

What we're going to do now is review several case studies that demonstrate how estimating mass flux and discharge can add value at some of your own sites.

## **Frequency of Method Applications**

70



Mass Flux and Mass Discharge Measurement/Estimation Method	No. Sites Where Applied
Transects with groundwater sample collection	41
Integral Pump Test(s)	7
Transects with passive flux meters	5
Isoconcentration contours	2
Mass Balance	2
Solute Transport Model	1

This table lists the frequency that various methods were used to estimate mass flux and discharge in the published case studies.

We can see from this table that the most common method for estimating mass discharge is the use of transects with the collection of groundwater samples. This method is probably the most common because it's relatively simple to apply in the field.

From the published case studies, we have seen more recent use of integral pump tests to estimate mass discharge at transects, as well as passive flux meters.

Many of these reported case studies were specifically intended to compare methods for mass flux estimation or performance of an in-situ treatment technology.



The data for this site were published in a class mass flux paper written in 2001 by Einarson and MacKay and published in Environmental Science & Technology.

This contour map shows the distribution of concentrations of cis-1,2-DCE in a transect that is approximately 30 meters in length.

These data show the same trend that we have seen in other sites where high resolution monitoring has been conducted.

And more than 80% of the mass is situated in less than 7% of the transect.

Over 99% of the mass is situated in less than 30% of the transect cross-sectional area.

Identifying the core of the plume mass such as was done at this site can help to focus remediation and monitoring efforts which may result in substantial cost and time savings.



Next we'll talk about the Well 12A Superfund Site in Washington where mass discharge was negotiated as an interim remedial goal.

As part of the Focused Feasibility Study, groundwater modeling determined that a reduction in source strength of 90%, which represents an order of magnitude decrease, would be sufficient for compliance to be achieved through MNA.

So here's an example of a site where mass flux and mass discharge are being used not only as a performance metric to evaluate treatment efficiency, but also as a decision guide for when to transition from active treatment to MNA.



Our third example is a regional basin with a commingled PCE plume that was created as a result of multiple source sites throughout the basin.

The red symbols indicate locations of potential sources contributing to the commingled PCE plume in the basin.

The yellow zone represents the capture zone for the regional supply wells shown here in blue.

The purpose of mass discharge monitoring was to evaluate which sites required further investigation and remediation, and which sites required no further action.

In the basin, multiple transects of pumping were installed downgradient of specific sites. The southern transect had a negligible mass discharge, so it was decided that these potential source sites in the south were not a priority for further investigation.

This example where sources at multiple sites are prioritized, is analogous to what we see at larger sites where multiple source zones exist. At these large sites, we can use a similar approach to prioritize which source zones need immediate treatment, and which can either be designated as a lower priority or requiring no further action.



The fourth example, Reese AFB, is really interesting. This example was provided by Fred Payne at Arcadis.

Here's a site that back in 2004 had a 3-mile long TCE plume. Response to remediation had stagnated.

When Arcadis became involved, they recognized that more characterization of the source zone was needed to define how the mass was distributed.

This enhanced characterization of mass flux in the source zone resulted in the decision to focus active bioremediation where mass was highest in the source zone.

The enhanced mass flux characterization was also used to optimize the use of groundwater extraction wells to accelerate mass removal from the source zone.

This is an example of what Fred appropriately calls "Flux-informed decision-making", where the mass flux distribution was used to improve the efficiency of the remediation effort.

Through this effort the mass in the plume has been reduced by a factor of ten and is still decreasing today.











Links to additional resources: http://www.clu-in.org/conf/itrc/ummfmd/resource.cfm

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