

General Approach....

A parametric study is a mathematical exercise. Start simple and then add on additional factors to figure out what is important under different conditions....

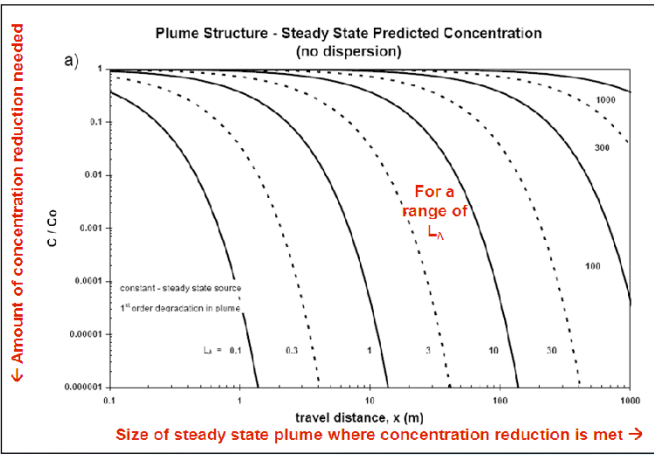
$x = \frac{v_s}{R} t = v_e t$ & $(C/C_0) = e^{-\lambda t}$
 plug flow w/ sorption degradation

$x = \frac{v_s}{R\lambda} \ln\left(\frac{C}{C_0}\right) = -L_\lambda \ln\left(\frac{C}{C_0}\right)$
 steady state plume

Full plume differential equation
 $R \frac{\partial C}{\partial t} = -v \frac{\partial C}{\partial x} + \alpha_x \frac{\partial^2 C}{\partial x^2} + \alpha_y \frac{\partial^2 C}{\partial y^2} + \alpha_z \frac{\partial^2 C}{\partial z^2} - \lambda C$

Assume steady state, neglect dispersion
 $0 = -v \frac{\partial C}{\partial x} - \lambda C$ $\frac{dC}{dx} = -\lambda / v C$
 at $x=0, C=C_0$

Solution
 $\ln \frac{C}{C_0} = \frac{-\lambda x}{v}$



What does the math tell us...

- The magnitude of concentration reduction needed is a key determinant of maximum plume size and the timeframe of plume cleanup
- The rates of attenuation processes in the plume strongly impacts the ultimate size of the plume
- Confirmed EPA preference for degradation processes. Degradation is a dominant natural attenuation mechanism, but any mechanism (anaerobic, aerobic or abiotic) can contribute.
- Source decay and source remediation can reduce plume size (but not as much as you might expect)
- Sorption is not a dominant mechanism unless the source is very short lived (and is mathematically less important if the sorbed material is assumed to be not degrading)
- Longitudinal dispersion is not an important attenuation mechanism and can increase plume length in some cases
- Transverse dispersion can contribute to attenuation if there is a basis for the spreading – but only for large plumes > about 1000 m



What does this math tell us...

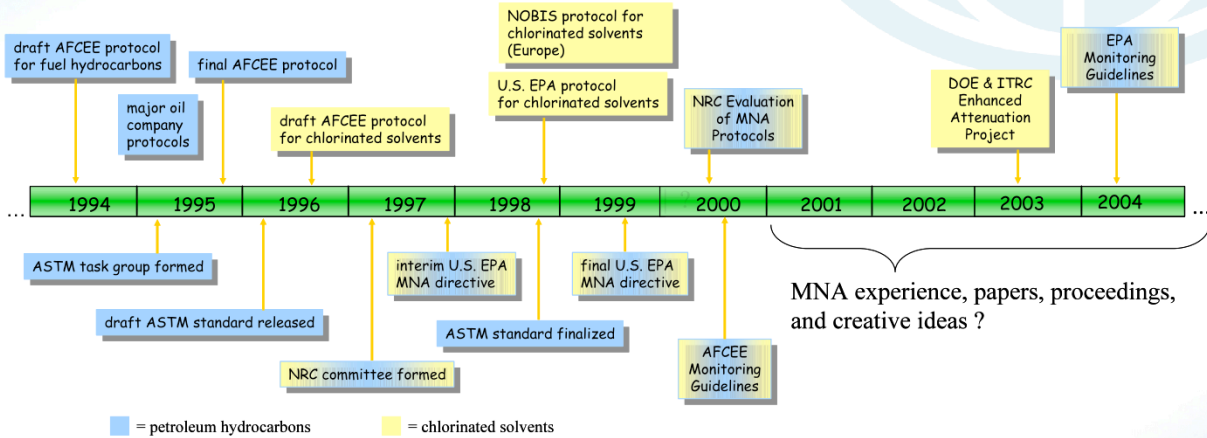
For Large and Dilute Plumes the size and scale of the steady state plumes will be larger than anaerobic sites. Best case aerobic plumes (weak sources and half lives of about 10 years) will stabilize within 1,000m (less than 1 mile) and “worst case” aerobic plumes (strong sources and half lives of 30 years) will stabilize within about 5,000 to 10,000m (about 3 to 6 miles)

This is what we see in real-world plumes!



Traditional Timeline for Natural Attenuation

Natural Attenuation of hydrocarbons and chlorinated solvents



Note: the major focus for chlorinated solvents is anaerobic processes



Dominant chlorinated solvent degradation mechanism(s) in aerobic aquifers based on recent literature

abiotic degradation with reactive mineral phases such as iron sulfides, magnetite (applicable to trichloroethene, carbon tetrachloride, etc.)

John Wilson et al. (EPA Laboratory Ada Oklahoma)

aerobic cometabolism (trichloroethene, etc.)

Hope Lee, et al (PNL Richland WA)

aerobic direct metabolism (dichloroethene, vinyl chloride, etc.)

Paul Bradley, et al. (USGS Columbia SC)

hydrolysis (carbon tetrachloride, etc.)

Peter Jeffers, et al. (SUNY-Cortland)



Abiotic Degradation – reactions dissolved plume with mineral phases

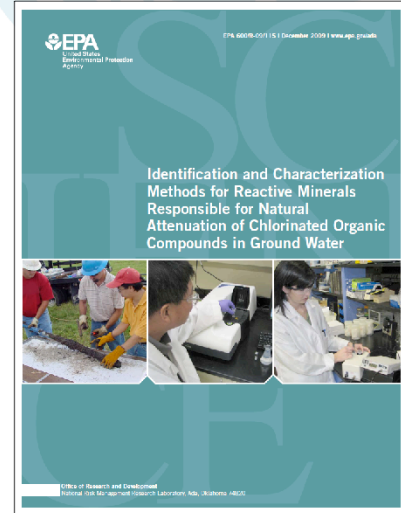
Types of minerals

reactive iron(II) minerals such as pyrite,
mackinawite (sulfides), Siderite (carbonate)

mixed iron(II) / iron(III) minerals such as
magnetite, green rusts, and goethite

mixed iron(II) / titanium (IV) minerals such
as ilmenite

For several real sites, significant attenuation
has been documented due to magnetite and
rates have been correlated to inexpensive
magnetic susceptibility measurements --
half lives of 3 to 6 years measured at sites
with magnetite present



EPA 600/R-09/115

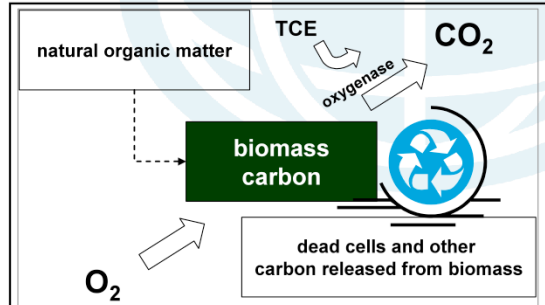


Summary of aerobic cometabolism research

Half lives of about 10 to >40 years have been measured

Based on current conceptual model the natural attenuation processes appear sustainable and are consistent with the expected microbial ecology of oligotrophic (nutrient limited) systems

SRNL/INL/PNL team currently working on long-lived “natural organic carbon” amendment technology to sustainably enhance aerobic cometabolic rates in L&D settings



Conceptual “Microbial Ecology” Model: We have shown that oligotrophic aquifers typically have significant numbers of organisms that are producing cometabolic oxygenase enzymes – approximately 10^4 (10^3 to 10^5) cells per mL. Since recycle of carbon is not 100% efficient (i.e., O_2 to CO_2), slow oxidation of natural organic matter provides the organic carbon necessary to sustain the microbial communities. Aromatic-rich natural organic matter induces the expression of oxygenases that have been documented to cometabolize TCE and other solvents. For large aerobic plumes, understanding this and other aerobic degradation processes and rates is crucial to successful environmental management because it bounds the requirements for source and primary plume treatment needed and facilitates transition to natural attenuation.

hypothesis

Putting it together (REMChlor example)

REMChlor Remediation Evaluation Model for Chlorinated Solvents User's Manual

by

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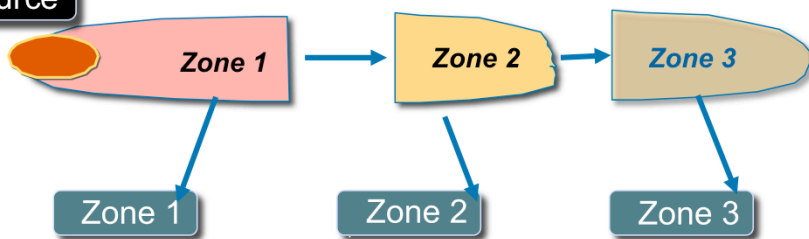
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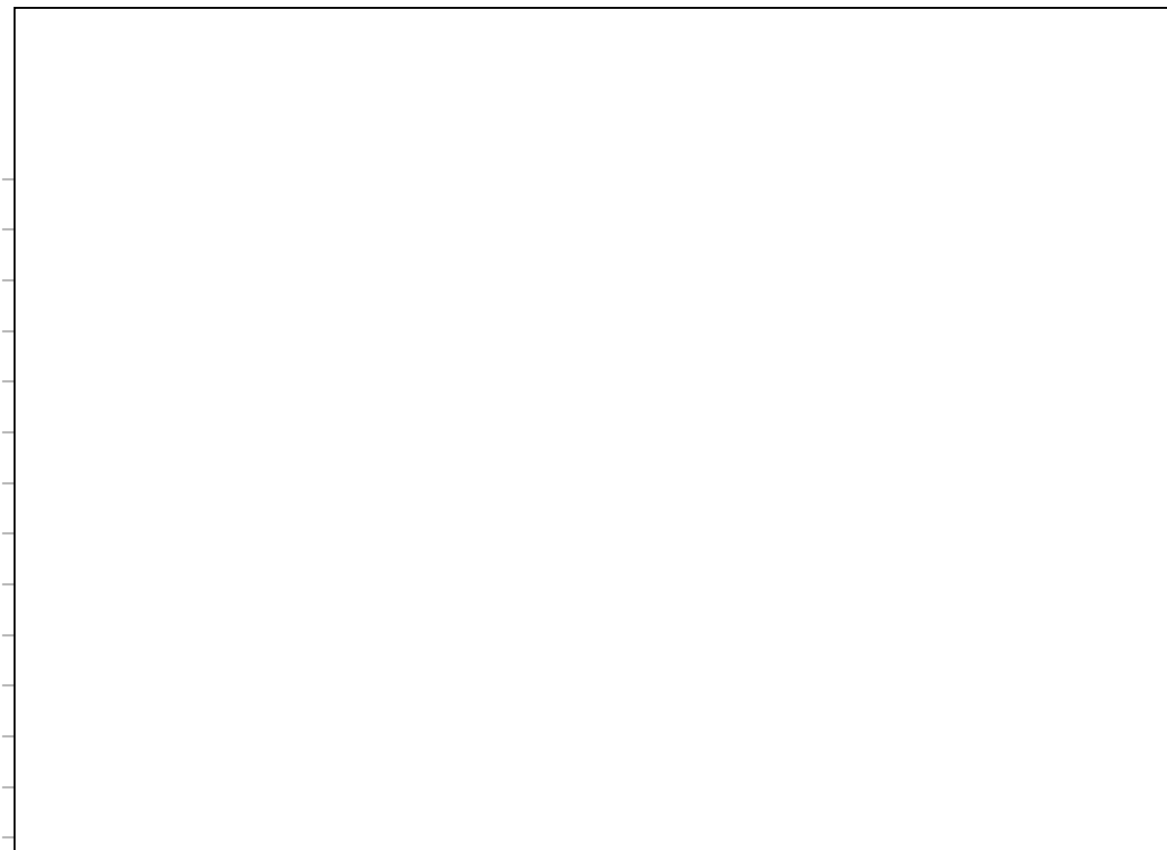
Conceptualization (REMChlor example)

Source Remediation plus Three plume Reaction Zones that Vary over Time

Source

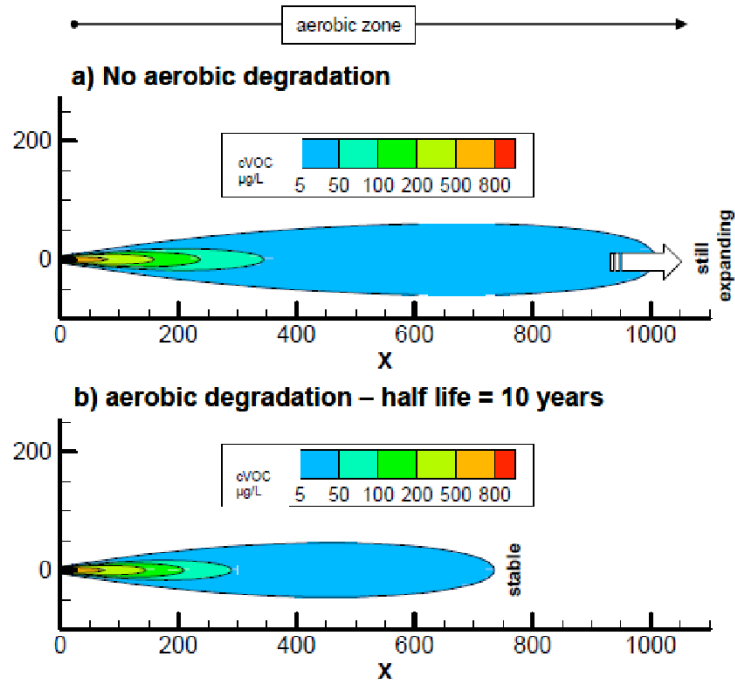


Often Low or Background Decay Rates



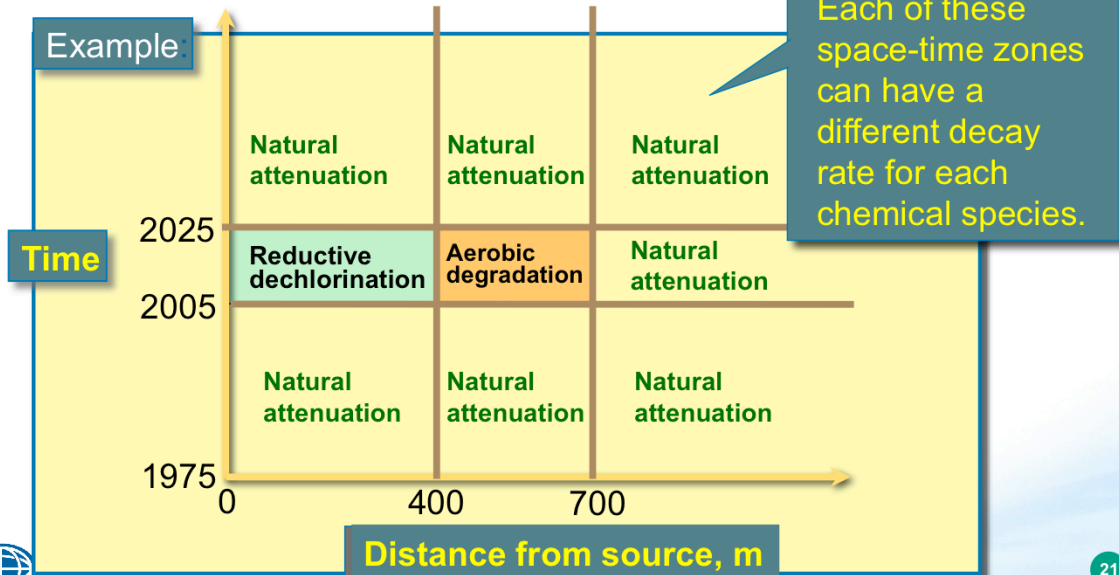
Simple example for natural attenuation

- 200 kg release
 - $C_o = 1000 \text{ ug/L}$
 - Pore velocity = 60 m/yr
 - Anaerobic ... 0 to 20 m
 - Remainder ... aerobic
-
- A conservative assumption of no degradation in the aerobic zone results in plume expansion for approximately 60 years (plume length > 1000m)
 - An assumed aerobic zone half life of 10 years stabilizes the plume earlier (plume length about 750m)



REMchlor “space-time structure”

Divide space and time into “reaction zones”, solve the coupled parent-daughter reactions for chlorinated solvent degradation in each zone; for example:



ORNL

RemChlor Input Screen

REMChlor - [REMChlor Model Parameters]

File Model Help

- Project: basecase
- Model Parameters
- View Model Results
- View File Output
- View Graphical Output
- Output vs. Distance
- 2D Contour

Source Zone Parameters

Source Parameters

Initial Source

Concentration (g/L)

Mass (Kg)

Gamma

Source Dimensions

Source Width (m)

Source Depth (m)

Darcy Velocity (m/yr)

Porosity

Source Remediation

Fraction Removed

Remediation Time

(Years)

Start Time (T1) End Time (T2)

Source Decay (1/yr)

Transport Parameters

Retardation Factor

Velocity

Sigmav vMin vMax

Number of Stream Tube

alpha (m) alpha (m)

	Yield 2 From 1	Yield 3 From 2	Yield 4 From 3
Component 1	<input type="text" value="0.6485"/>	<input type="text" value="0"/>	<input type="text" value="0"/>
Component 2	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Component 3	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Component 4	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>

Component Name

	Zone 1	Zone 2	Zone 3
Decay Rate (1,3)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (2,3)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (3,3)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Period 3	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>
Decay Rate (1,2)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (2,2)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (3,2)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Period 2	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>
Decay Rate (1,1)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (2,1)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Decay Rate (3,1)	<input type="text" value=""/>	<input type="text" value=""/>	<input type="text" value=""/>
Period 1	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>	<input type="text" value="0.34"/>

Time, Years

40
Time -->
Period 2

30
Time -->
Period 1

Distance From Source, Meters

×1

×2

Cancer Risk

Lifetime Oral Cancer Risk | Lifetime Inhalation Cancer Risk

	Component 1	Component 2	Component 3	Component 4
Lifetime Oral Cancer Risk	<input type="text" value="0.091"/>	<input type="text" value="0"/>	<input type="text" value="0"/>	<input type="text" value="0"/>

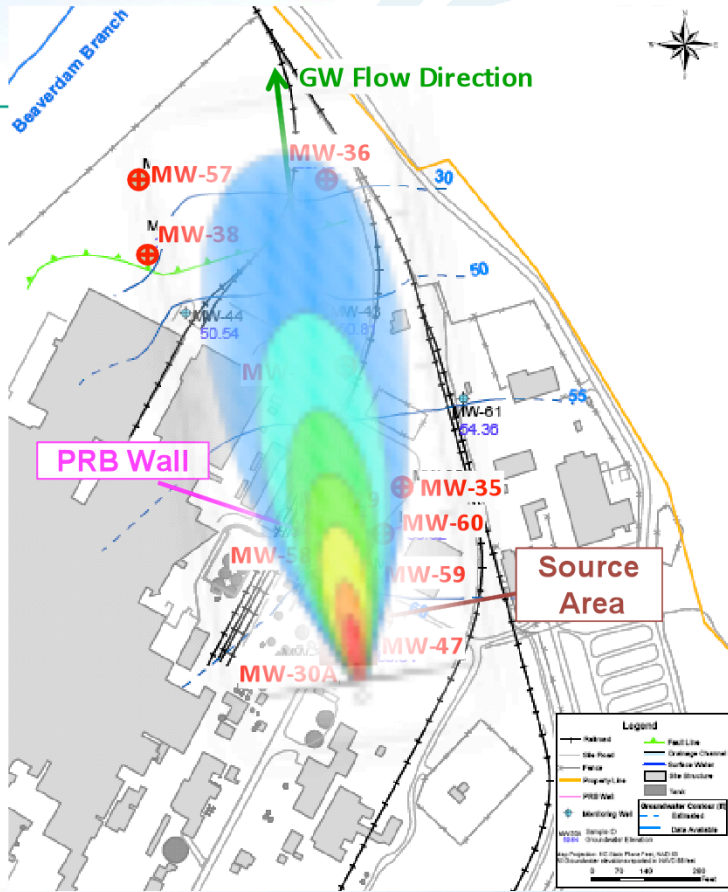
Simulation Parameters

	Intervals	Min Value	Max Value	Units
X - Direction	<input type="text" value="101"/>	<input type="text" value="0.01"/>	<input type="text" value="500"/>	Meter
Y - Direction	<input type="text" value="41"/>	<input type="text" value="-60"/>	<input type="text" value="60"/>	Meter
Z - Direction	<input type="text" value="1"/>	<input type="text" value="0"/>	<input type="text" value="0"/>	Meter
Time	<input type="text" value="50"/>	<input type="text" value="0"/>	<input type="text" value="100"/>	Year

DNAPL Source Zone → Dissolved Plume

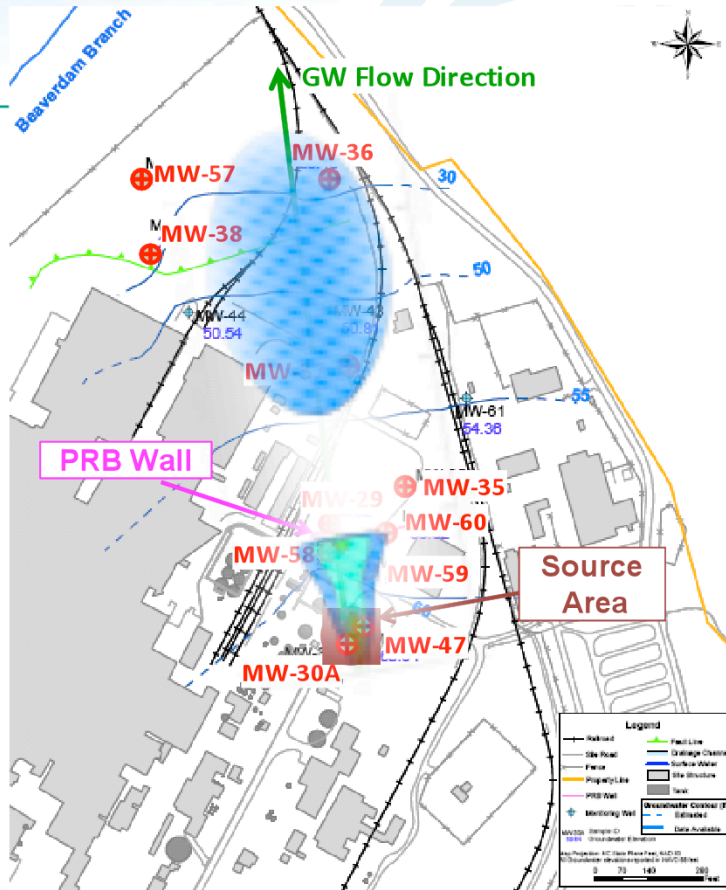
Simulated TCE concentrations
 In 1999 prior to
 source
 remediation
 or PRB wall
 installation

Contours at
 5, 20, 50, 100,
 200, 500, and
 1000 ug/L



**Simulated TCE concentrations
In 2009, 10
years after
source
remediation
and PRB wall
installation**

**Contours at 5,
20, 50, 100, 200,
500, and 1000
ug/L**



Some trends in recent modeling results

The concentration reduction required to meet interim or final goals is linked to the amount of source removal needed

The solubility of the source DNAPL strongly impacts the remediation timeframe (e.g., timeframe for PCE >> TCE)

A 90% source reduction does not reduce plume size by 90% -- this type of reduction often has little effect on the ultimate size of the 5ppb contour but a relatively large impact on the 100ppb contour.

Modeling confirms the value of source remediation (combined remedies) but effects on the distal portion of the plume requires time for the impacts to wash through – mass transfer will further extend timeframes



Overarching Goal Setting Concepts (from the REMchlor workshops)

The goal of remediation is to protect human health and the environment to the extent practicable.

The ultimate objective is to restore the impacted resource and the services that the resource provides (ecological, drinking water, etc.)

A binary metric (pass-fail) for success may discourage clean-up

A variety of metrics for interim goals were explored -- mass flux is an example metric to link source treatment and plume impacts – new concepts such as the “Plume Magnitude Scale” are emerging – risk reduction – optimization functions – etc.



Summary for Goal Setting

Interim source/mass balance objectives may be useful for DNAPL source treatments and tie into “combined remedy” constructs

“impacts on the 5 ppb contour are a weak metric for success of a source or central plume treatment”

“mass flux to the plume to a predetermined level may be a good interim metric”

“impacts on plume structure (e.g., the 100 ppb contour) are more diagnostic metrics of the success of source treatment”

Other regulatory and legal constructs may be needed (e.g., natural resource damage assessment) to effectively compensate for lost resources/services.

Need to apply realistic timeframes

Technical impracticability ? ☹️



Finishing up -- M Area Example from the DOE Savannah River Site

Quick facts:

2013 is the 30th anniversary of pump and treat at this site

15 years of soil vapor extraction

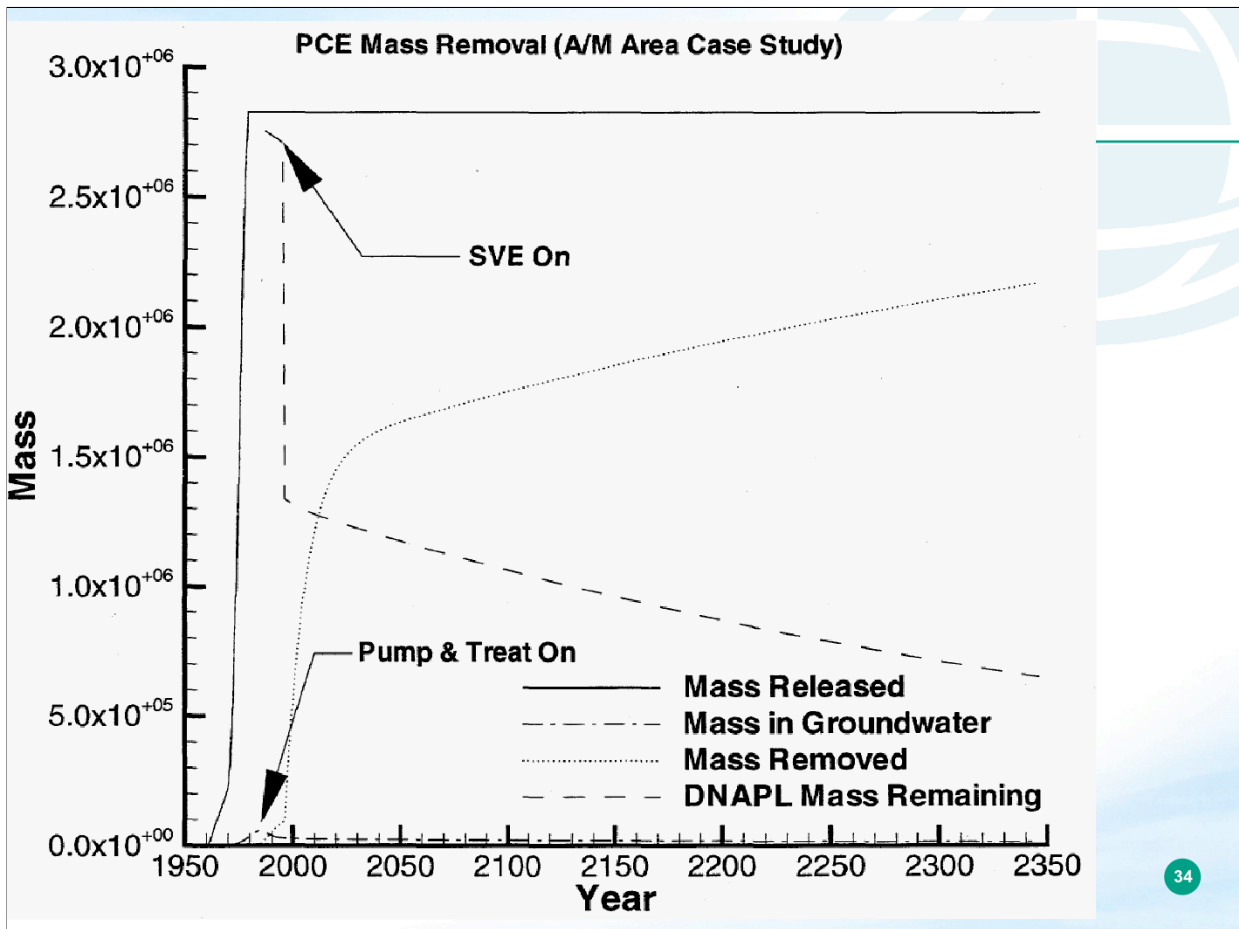
Thermal remediation (steam) of solvent storage tank and M Area Basin

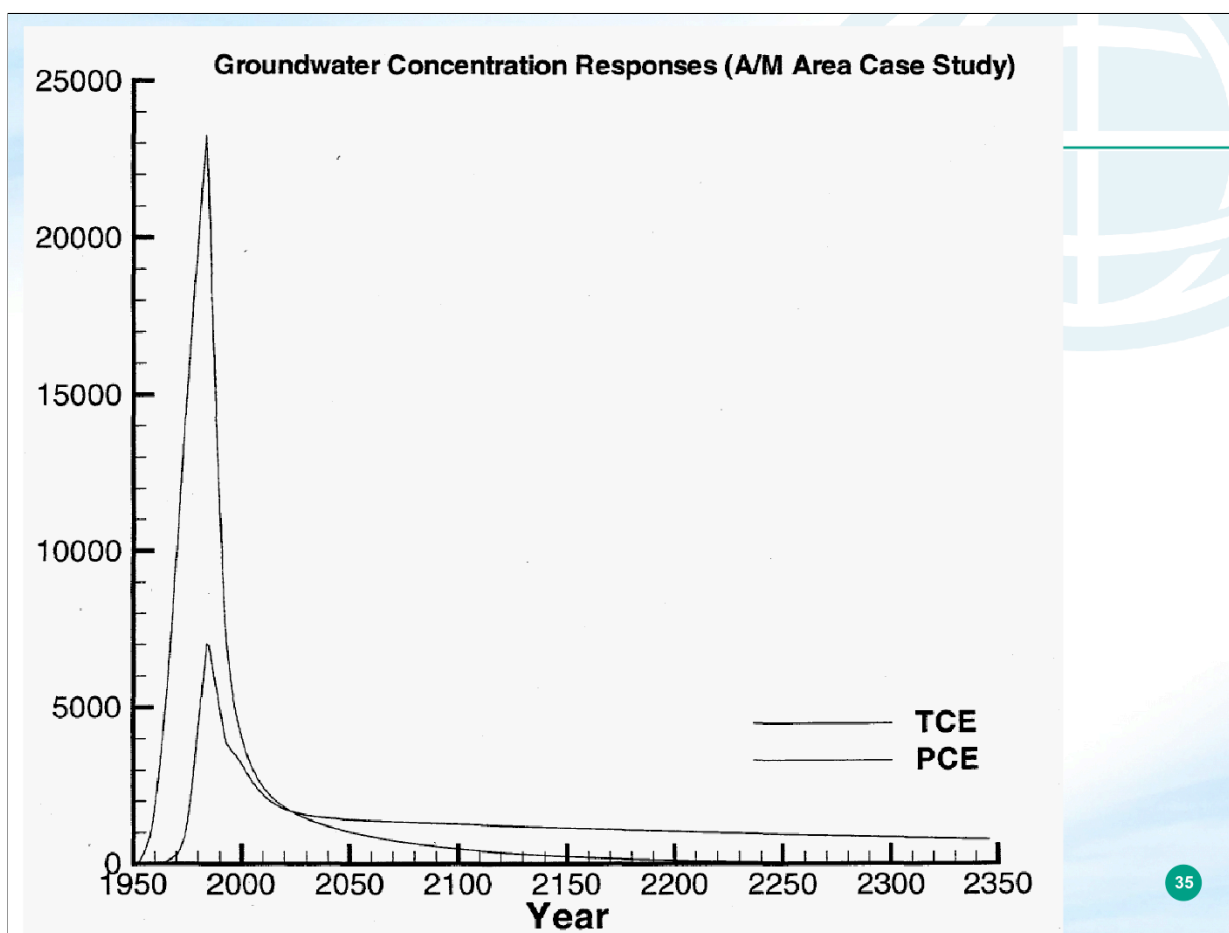
Pilot testing of air sparging, cometabolic bioremediation, Electrical resistance heating, radio frequency heating, oxidants, etc.

Finish up with a quick final look at a real large dilute plume remediation

Start with an early mass balance model for source and plume remediation and compare to some current inventories





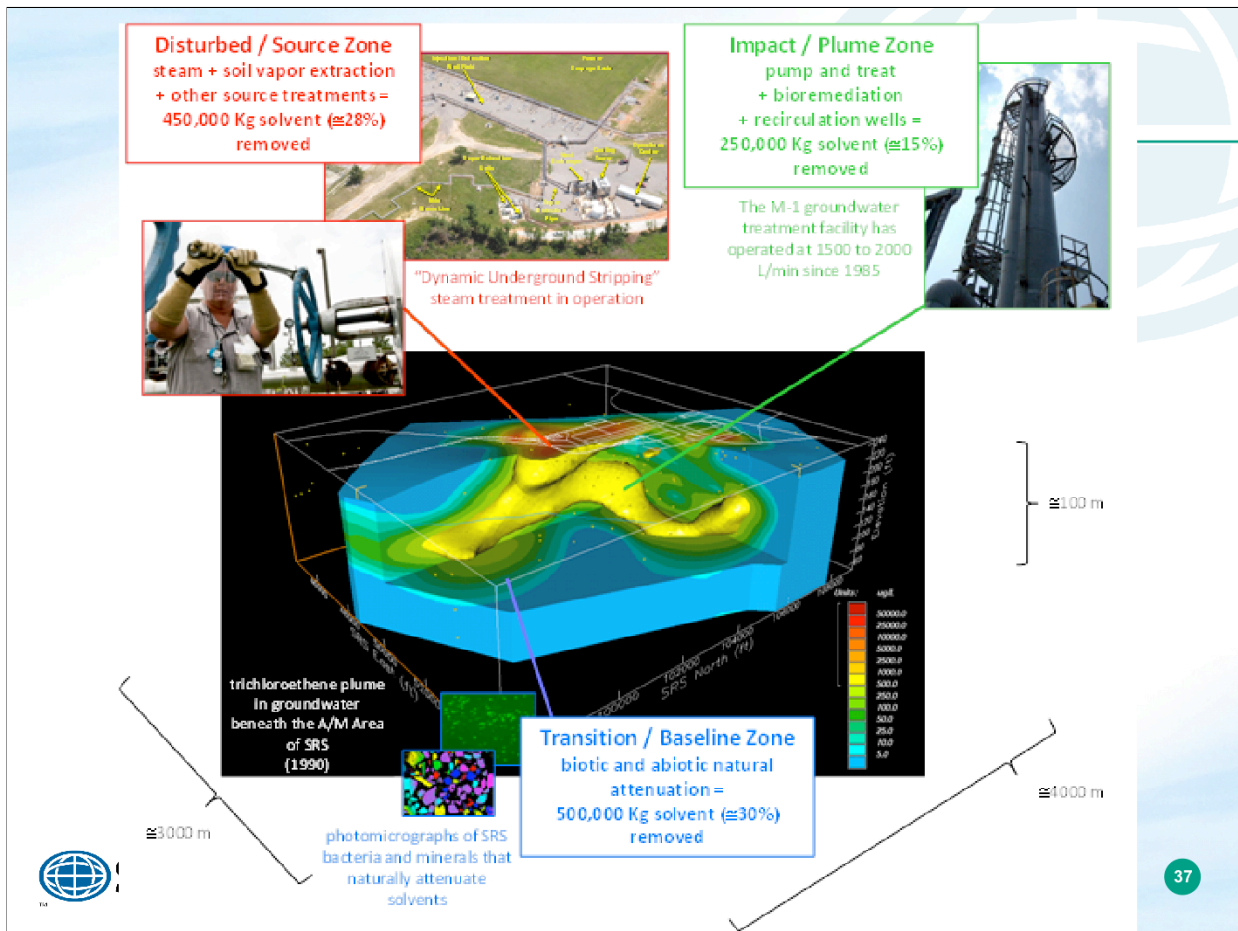


M Area totals

Dennis Jackson is currently preparing a paper on M Area (in honor of the 30th anniversary). Preliminary tally numbers...

	lbs	% removal based on total from active treatments	% removal based on total est. release of 3.5 million lbs
Pump and Treat	490000	33%	14%
Soil Vapor Extracton	448000	30%	13%
Field Testing	36000	2%	1%
Recirculation Wells	5700	0.40%	0.20%
Steam / Thermal	508163	34%	15%
Total from all active	1490000	100%	42%
MNA (40 yr half life)	1230000	na	35%
Grand Total	2717098	na	78%





Conclusions – Challenges

Large and Dilute!

Aerobic – relatively slow (“weak”) attenuation rates for chlorinated solvents

Deep

Persistent plumes with long tails due to mass transfer processes

Requires clean-up of source zones coupled with other actions and time

Any treatment must provide sustainable (long-lived) performance and be deployable to impact a large area for a reasonable cost

Treatments should avoid large scale adverse collateral impacts when possible



Conclusions -- Opportunities



Remediation “successes” will:

- match technology and deployment to site specific conditions
- focus on actionable characterization data for a reasonable cost
- set technically-based, realistic and achievable goals
- link source treatment to desired impacts in the downgradient plume
- combine technologies as needed

Weak to moderate source strength, high permeability, presence of reduced iron minerals, presence of microorganisms that produce oxygenase enzymes, and other factors increase the potential for success in these challenging plumes

There is lots of emerging science: Abiotic processes may be “significant” at some/many sites; aerobic cometabolism occurring at most sites and rates appear to be related to microbial measurements

The breadth of work on remediation amendments may lead to attenuation enhancement materials that are viable for L&D conditions



Questions and Discussion



For more information, contact:

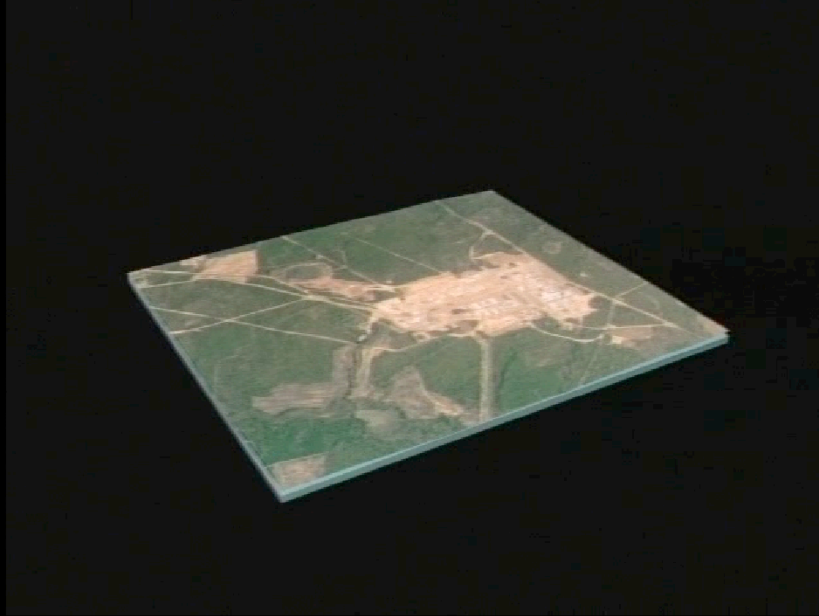
brian02.looney@srnl.doe.gov

or

fred.payne@arcadis-us.com



**An example “Residual Source”
process sewer line at the A/M Area of SRS**



video
