

# Assessment of Hydraulic Capture Through Interpolation of Measured Water Level Data

Matthew Tonkin<sup>1,2</sup>, Steven Larson<sup>1</sup> and  
Chris Muffels<sup>1</sup>

1. S. S. Papadopoulos & Associates, Inc.

2. University of Queensland, Australia.



*"Accelerating Site Closeout, Improving Performance, and  
Reducing Costs Through Optimization" - Dallas, Texas*

# Outline of This Presentation

- A Problem Statement
- Some History and Motivation
- A brief introduction to Kriging
- Some Reality Checks to be mindful of
- The inclusion of Particle Tracking
- A single illustrative Example

# Background and Developments

- The basis of the approach described here – combining kriging and hydrology – is an area of extensive historical investigation and literature
- This presentation discusses one fairly recent development in particular
- **David Dougherty** will discuss extensions to the approach described here that he has developed and applied

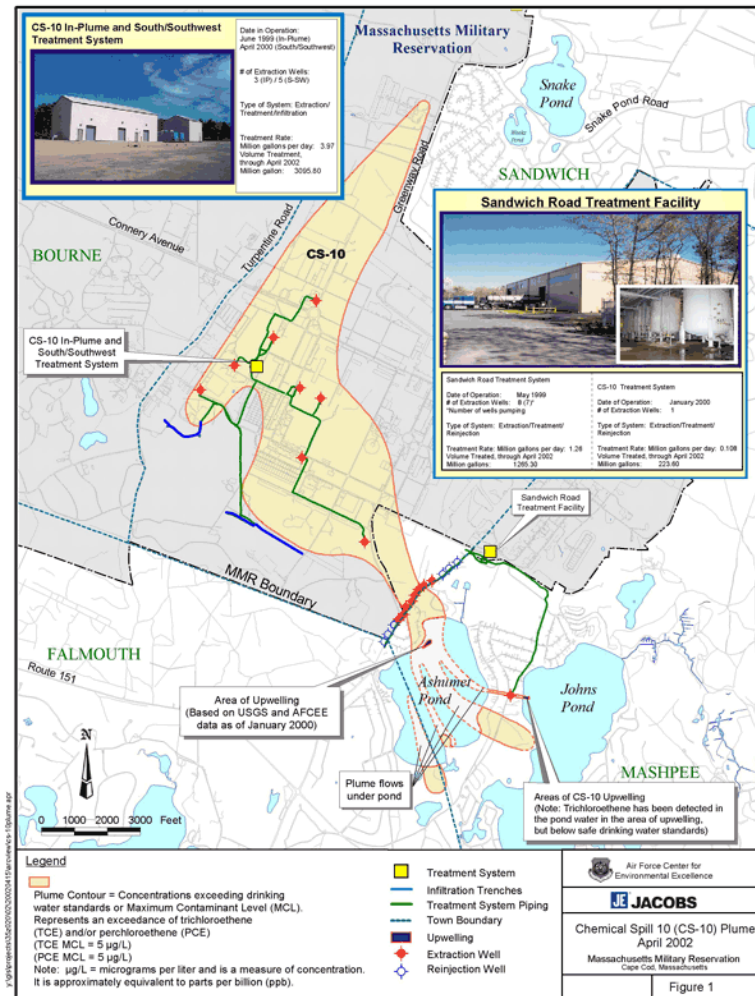
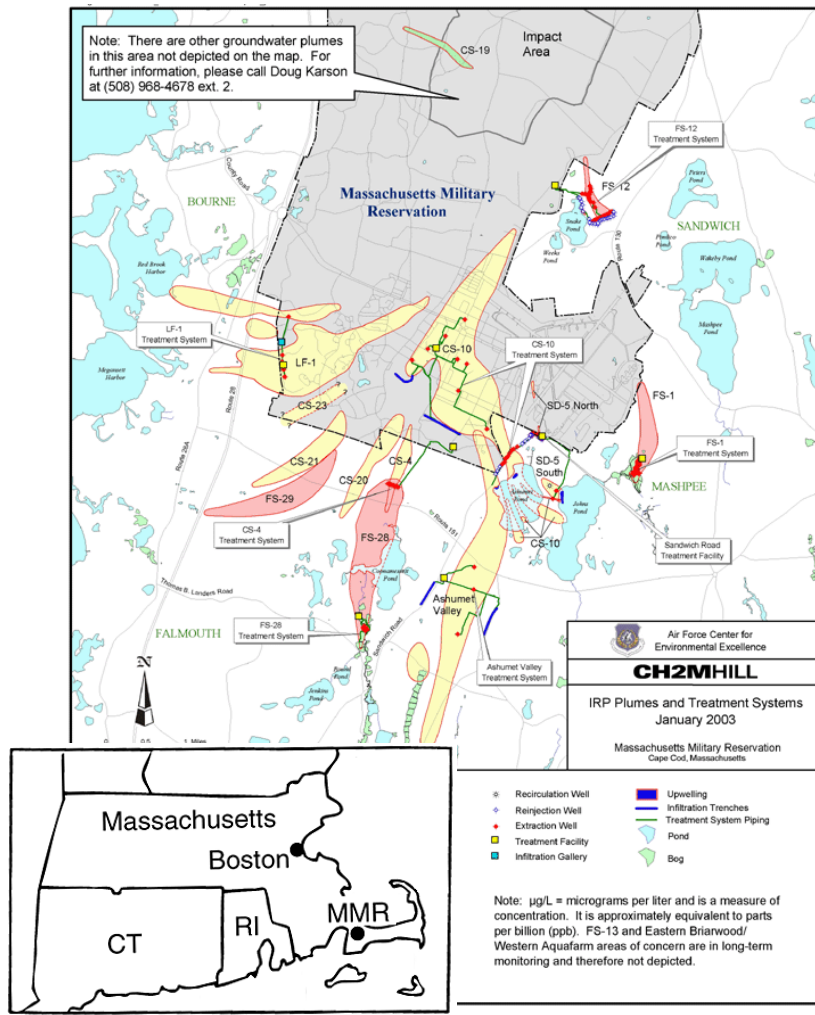
# Problem Statement

- How do we improve the inference that can be drawn from a water level data set?

# History

- OTIS-MMR, MA., 1998.
- Rapid development of several large-scale, multi-well pump-and-treat (P&T) remedies.
- Various options for returning treated water including injection, infiltration.
- Quarterly monitoring reports.
- Regular meetings.

# History



# History

- Common questions asked at these meetings.....
  - *How is the system performing?*
  - *Is capture developing?*
- The contents of quarterly reports were not intended to include capture zones.

# Making Maps

- Water levels are measured at a lot of wells - *but,*
- It is still necessary to interpolate between measured data in order to make maps - *and,*
- Most maps we make of water levels don't convey much information.



# Making Maps

- If we acknowledge that in order to make maps we must perform some form of interpolation - then,
- the question is which of the available methods is the most suitable for our needs?
  - inverse distance, kriging, radial basis functions, others?

# Motivation

- To increase the inference that can be drawn from water levels measured in monitoring wells

in order to

- Assist with inferring pump-and-treat system performance.



# Introduction to Kriging

- Kriging is a method for interpolating from known data to intermediate locations
- When rigorously implemented, interpolation weights are determined from the data
- Where there is assumed to be no measurement error, and there are no replicates, kriging is an exact interpolator
- Under certain assumptions about spatial statistics (variogram), kriging provides an estimate of the variance in the estimation error

# Some Bases for Kriging

- The variogram - intuitively, a descriptor for how information diminishes with separation distance.
- Linear algebra - a method for solving the matrix equations to estimate a point.

*Variography is fun - but can be taken too seriously .... data sets usually inadequate*



# Simple or Ordinary Kriging<sup>1</sup>

- Estimated value is a function of the surrounding, known data
- The weight given to the known data is proportional only to the separation distance of each known point from the estimation point

$$Z_{\text{est}} = f(R)$$

1. Assumptions about the mean of the quantify being estimated vary – for simple kriging, zero; for ordinary kriging, data average



# Kriging With a Trend<sup>1</sup>

$$Z_{\text{est}} = A + BX + CY$$

A = 'offset' term

B = gradient in the X direction

C = gradient in the Y direction

Trend coefficients must be linear

$$Z_{\text{est}} = f(X, Y, R)$$

1. Often termed 'Universal Kriging'



# Kriging With a Trend

- Kriging with linear trend has been shown to be effective in aquifer systems (e.g. Ogallala) where regional patterns are dominant.
- However – where we have singularities – such as wells – severe local departures from this linear trend occur.



# The Cooper-Jacob Equation

$$s = \frac{Q}{4\pi T} \ln \left( \frac{2.25Tt}{r^2S} \right)$$

$s$  = drawdown

$Q$  = pumping rate

$T$  = transmissivity

$S$  = storage

$r$  = separation distance

$t$  = time





# The Cooper-Jacob Equation

$$s = \frac{Q}{4\pi T} \ln \left( \frac{2.25Tt}{r^2S} \right)$$

s = drawdown

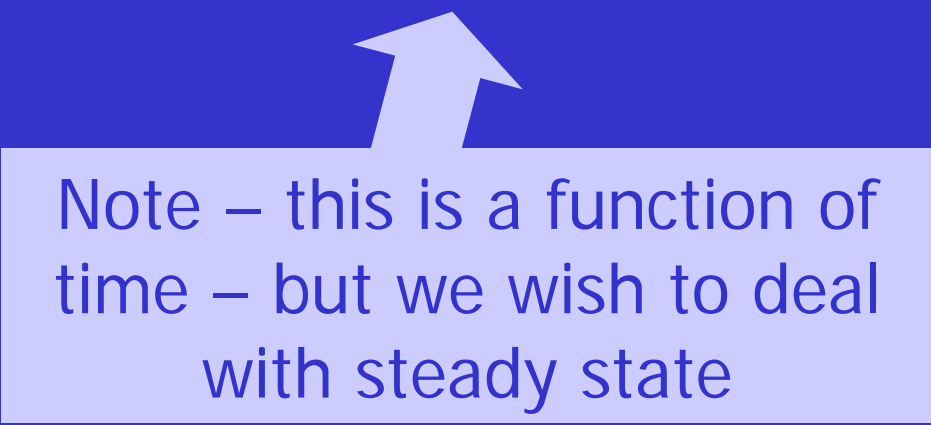
Q = pumping rate

T = transmissivity

S = storage

r = separation distance

t = time



Note – this is a function of time – but we wish to deal with steady state

# The Cooper-Jacob Equation

$$s = \frac{Q}{4\pi T} \left( \ln \left( \frac{2.25Tt}{S} \right) + \ln \left( \frac{1}{r^2} \right) \right)$$

This is a function of time

This is not

# The Cooper-Jacob Equation

$$s = \frac{Q}{2\pi T} \ln(r) \quad + \text{offset}$$

# The Cooper-Jacob Equation

$$s = \frac{1}{2\pi T} Q \ln(r) + \text{offset}$$

# The Cooper-Jacob Equation

$$s = \underbrace{\frac{1}{2\pi T}}_{} Q \ln(r) + \text{offset}$$

*Log trend coefficient*

# Multiple Extraction Wells

$$s_{ij} = \frac{1}{2\pi T} \sum Q_n \text{Ln}(r)_n$$

$s_{ij}$  = drawdown at  $(i, j)$  due to extraction

$Q_n$  = extraction rate at well  $n$

$\text{Ln}(r)_n$  = log of separation distance

$$Z_{\text{est}} = f(Q, X, Y, R)$$

# Reality Checks - Aquifer

- The estimated transmissivity should correspond with other sources of information - e.g. pumping tests.

and

- The estimated capture zone width should correspond with the estimated transmissivity, pumping rate, and hydraulic gradient.

# Capture Zone Width

$$W = Q / K B i$$

W = capture zone width

K = average hydraulic conductivity

Q = extraction rate

B = saturated thickness

i = hydraulic gradient

*Note: Half-width at the recovery well*





# Stagnation Point

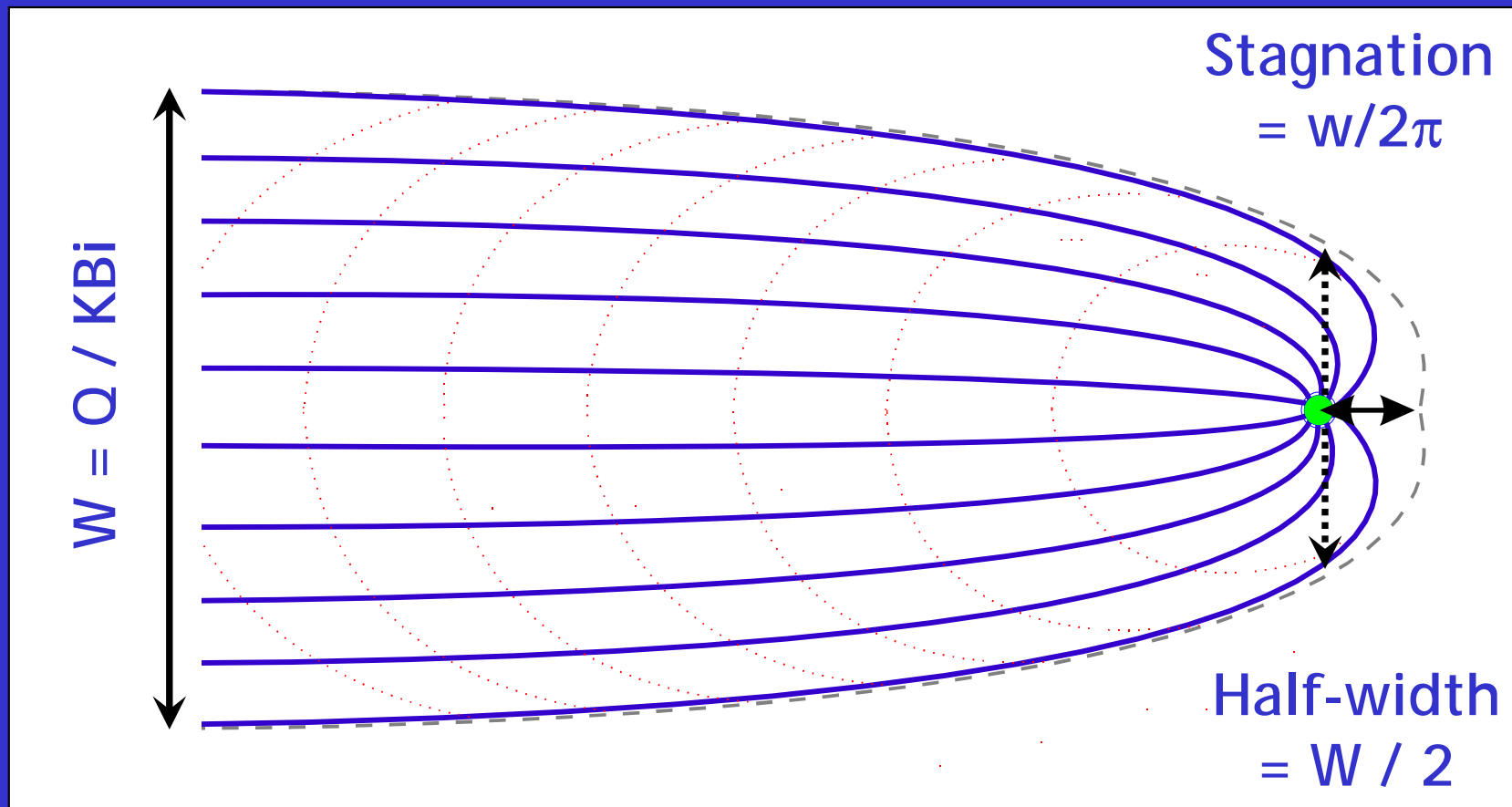
$$h = W / 2 \times \text{PI}$$

$h$  = distance of stagnation point down gradient of the recovery well

$W$  = capture zone width

$\text{PI}$  = 3.14159...

# Reality Checks - Aquifer



# Reality Checks - Data

- Do the data meet the assumptions
- Are there 'outliers' that require additional explanation
  - Jackknifing
  - Single-point cross-validation

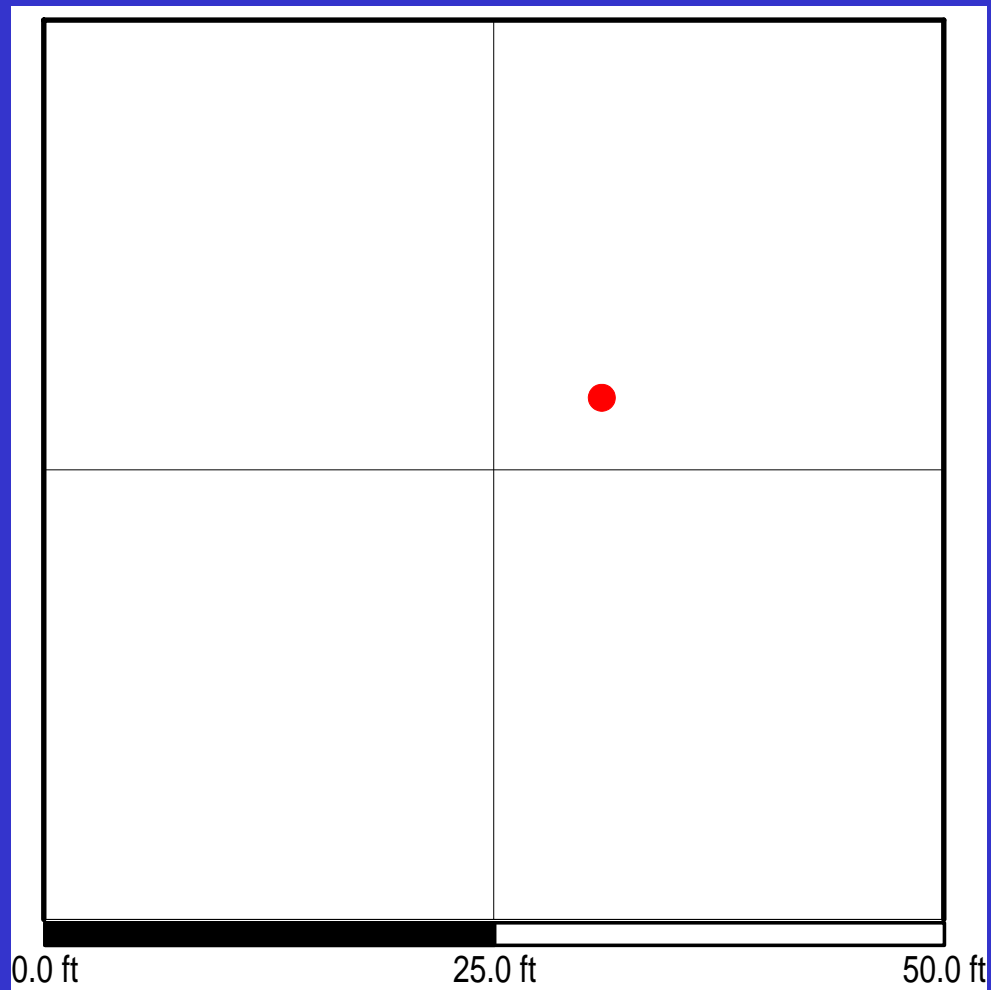
# Particle Tracking

Build directly from the kriging routine

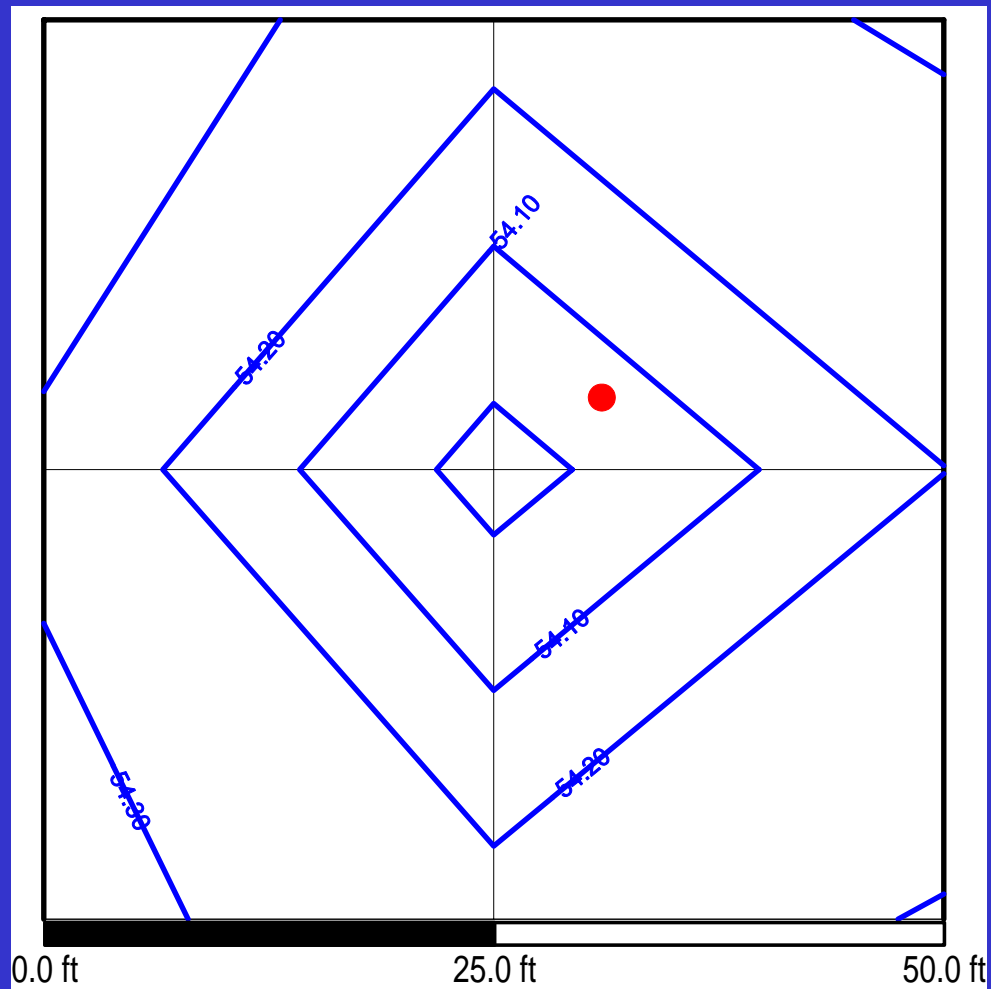
- Once the kriging matrix has been constructed the kriging weights that pertain to the estimation of any point are estimable
- The benefit of this approach is that the gradient and seepage velocity are calculated on the basis of the kriging estimate **exactly** at the location of the particle



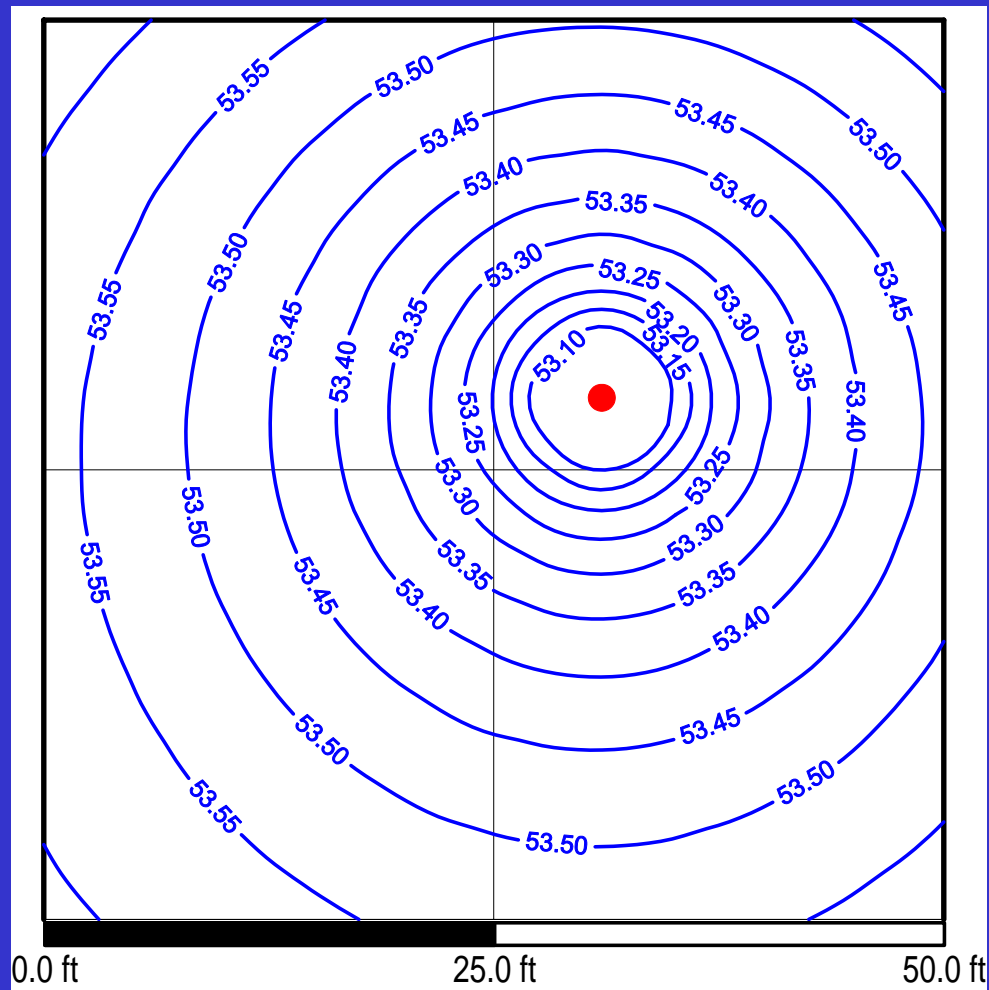
# Particle Tracking



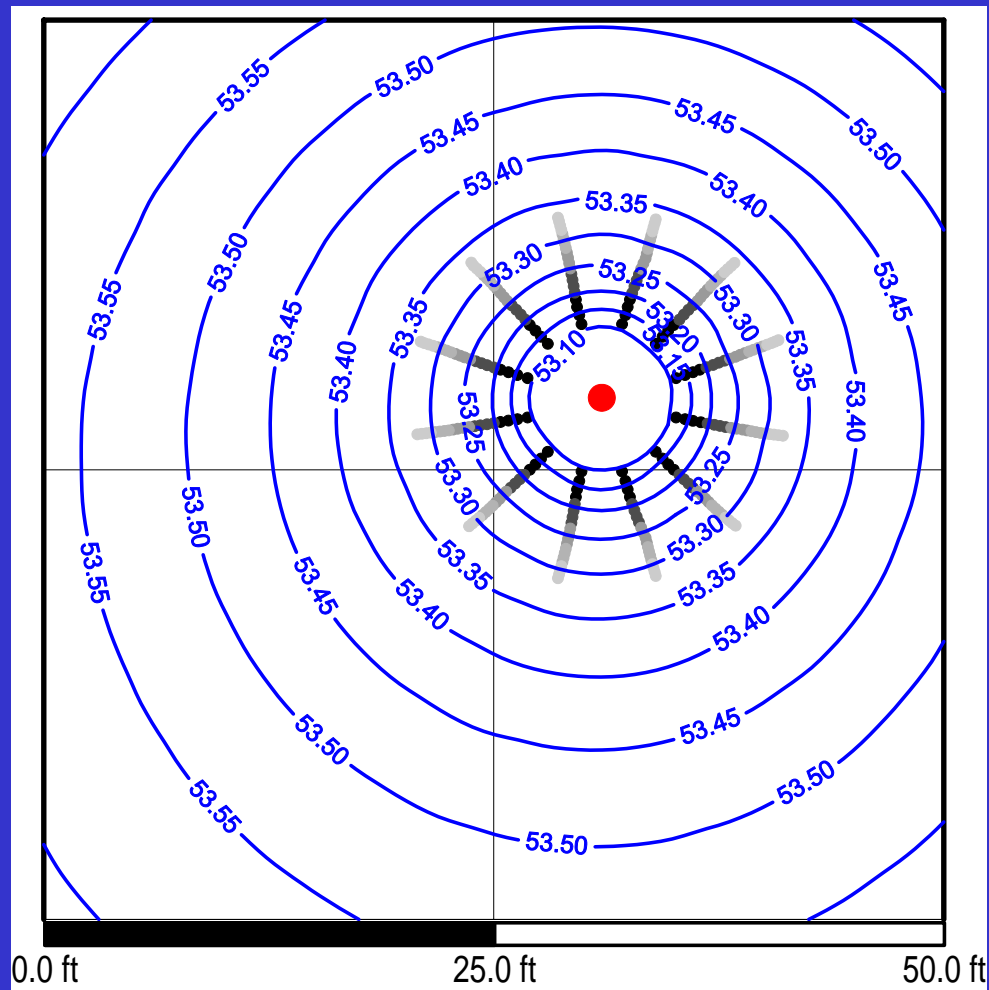
# Particle Tracking



# Particle Tracking



# Particle Tracking





# Example Application

## Cape Cod, MA.

- Described in the paper by Tonkin and Larson, 2002.

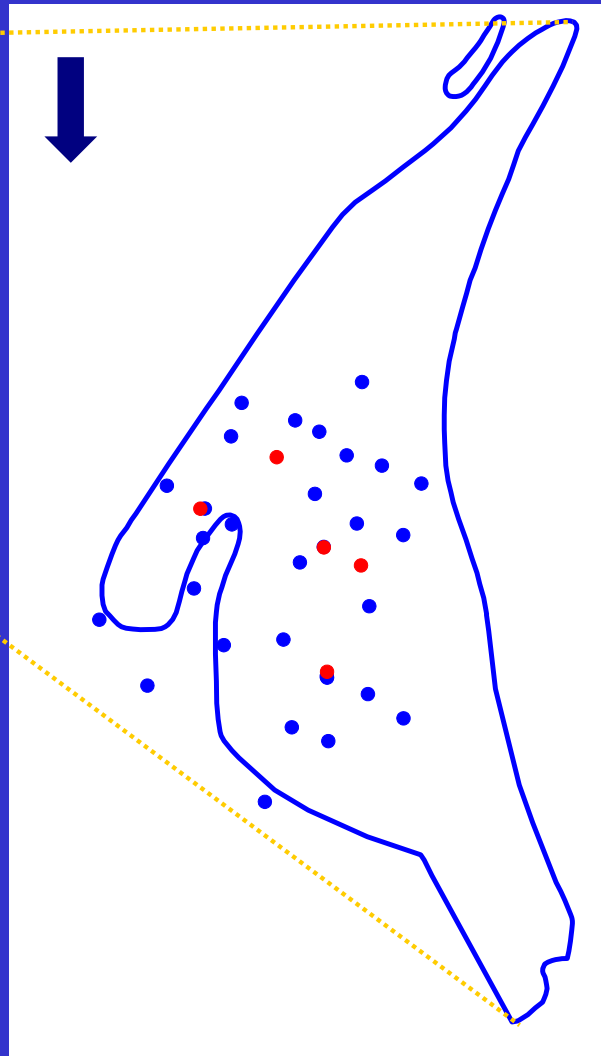
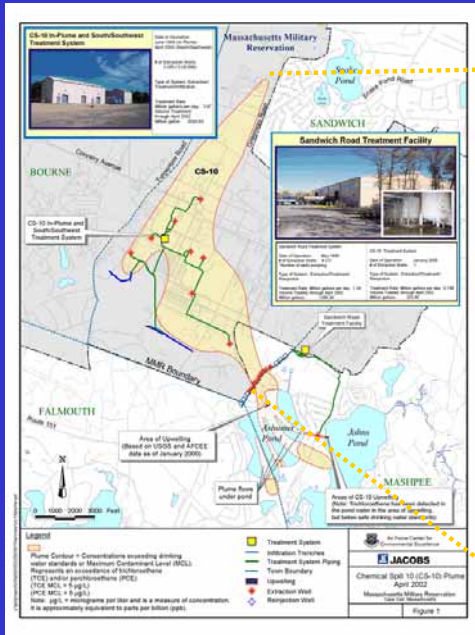


# Cape Cod

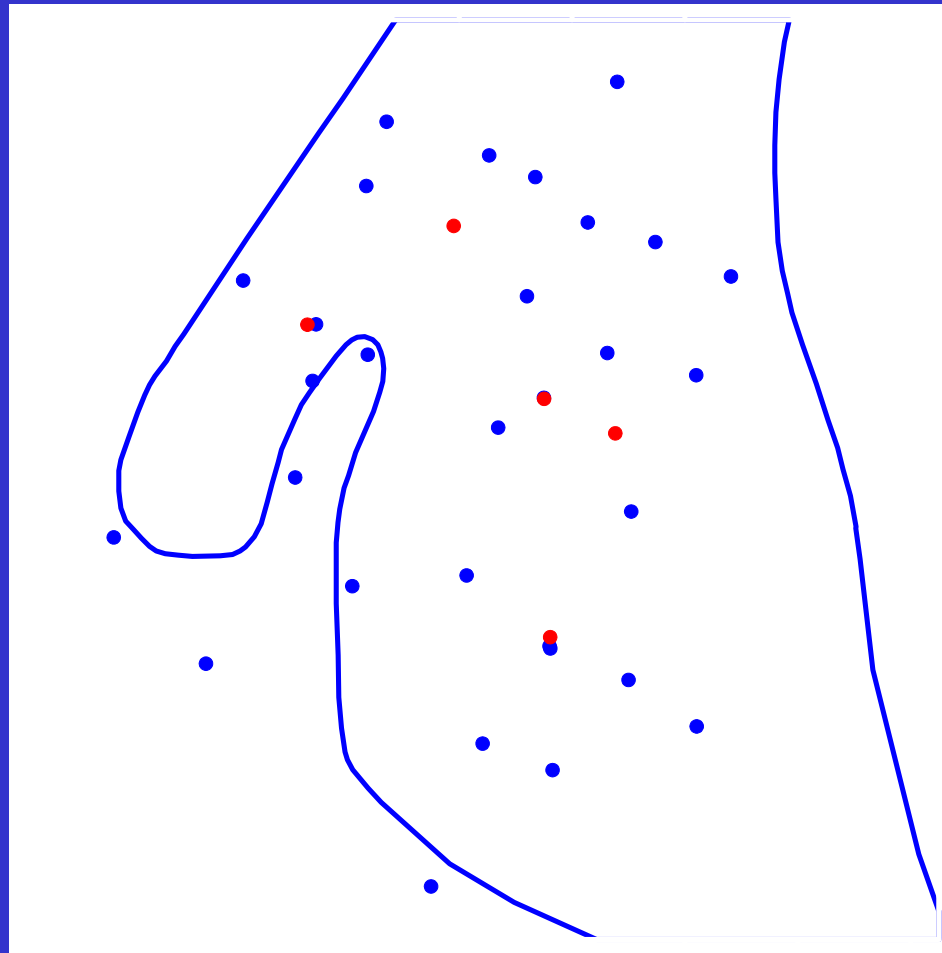
- CS-10 In-Plume System
- Mass recovery objective
- 5 extraction wells
- Peripheral infiltration galleries
- About 40 monitoring wells
- *Aim to infer if capture is developing*



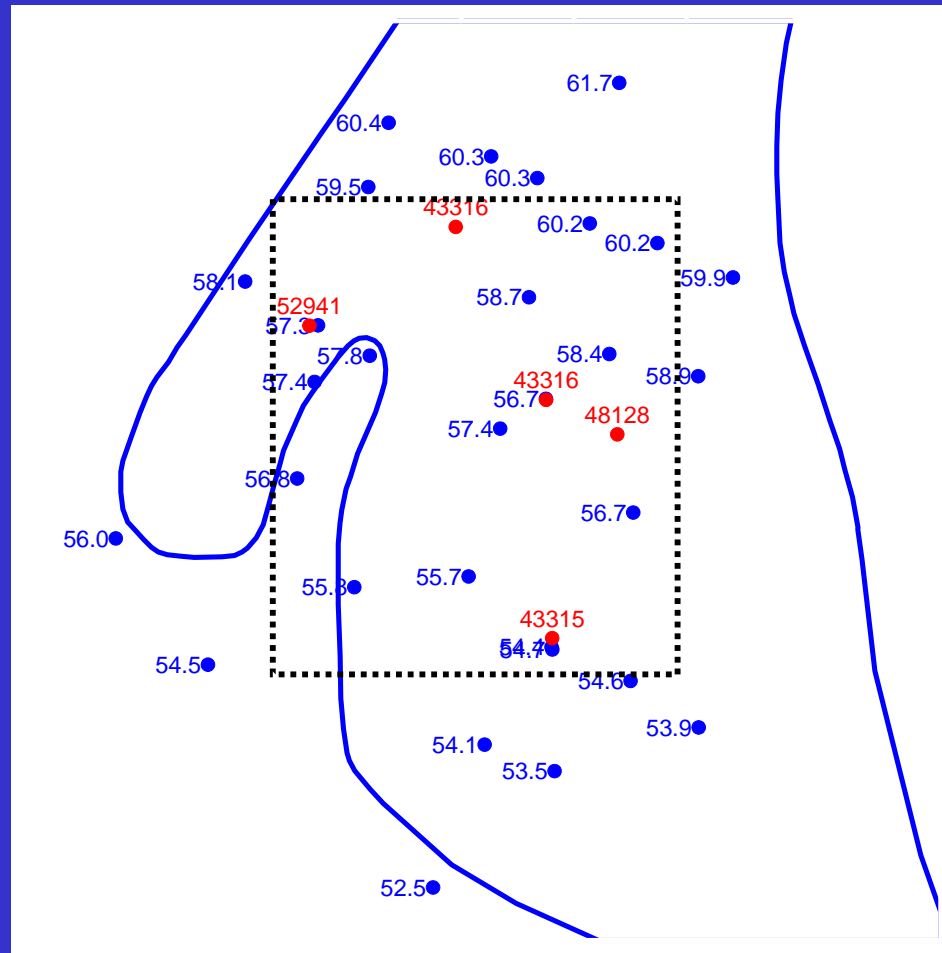
# Cape Cod - CS-10



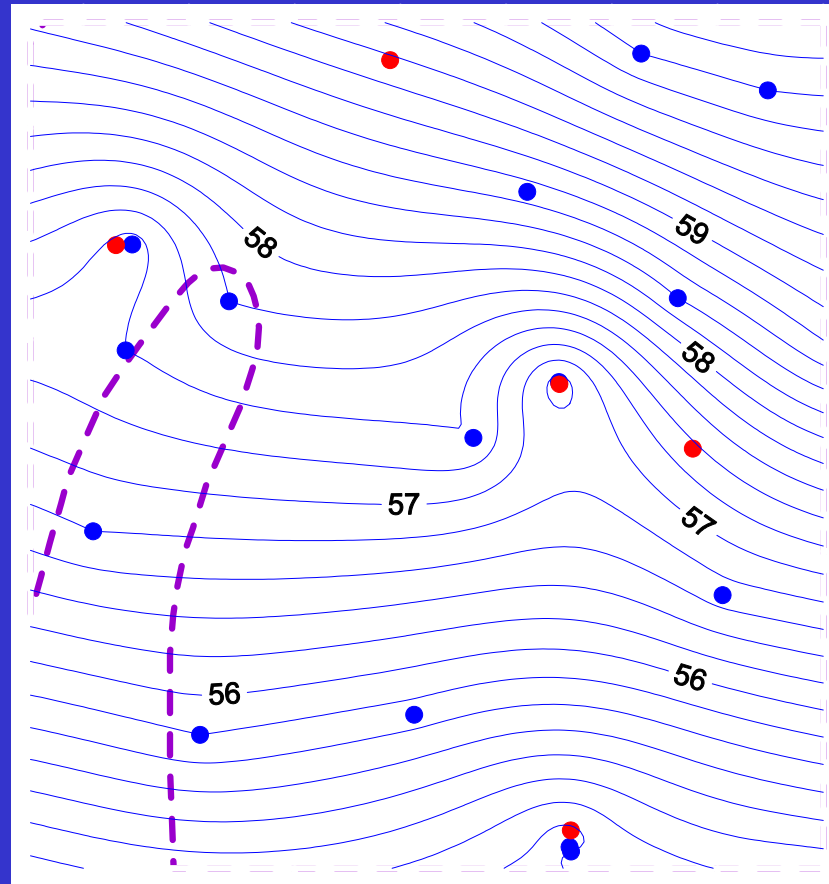
# CS10 - Zoom



# CS10 - Zoom

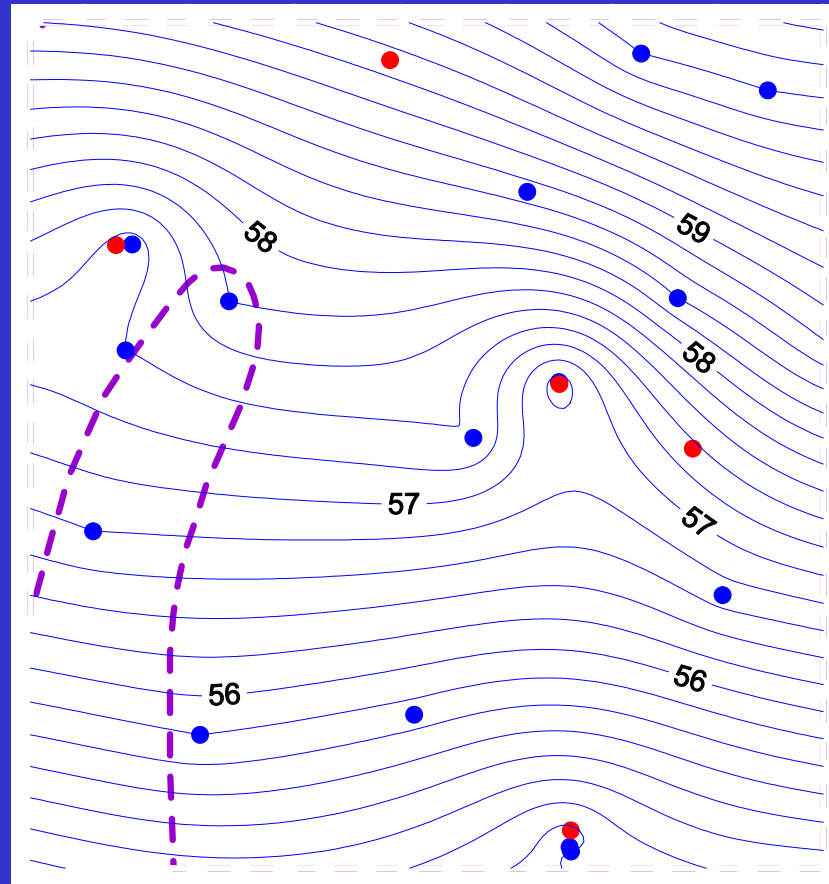


# Cape Cod - No Trend



$$Z_{\text{est}} = f(R)$$

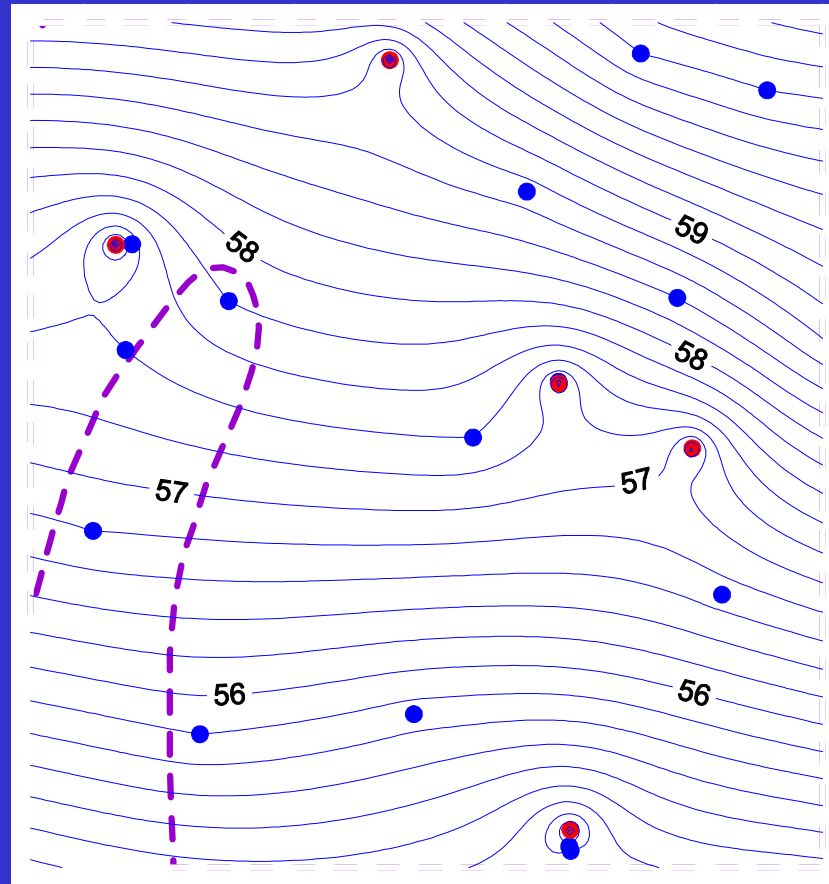
# Cape Cod - Linear Trend



$$Z_{\text{est}} = f(X, Y, R)$$



# Cape Cod - Linear-log Trend



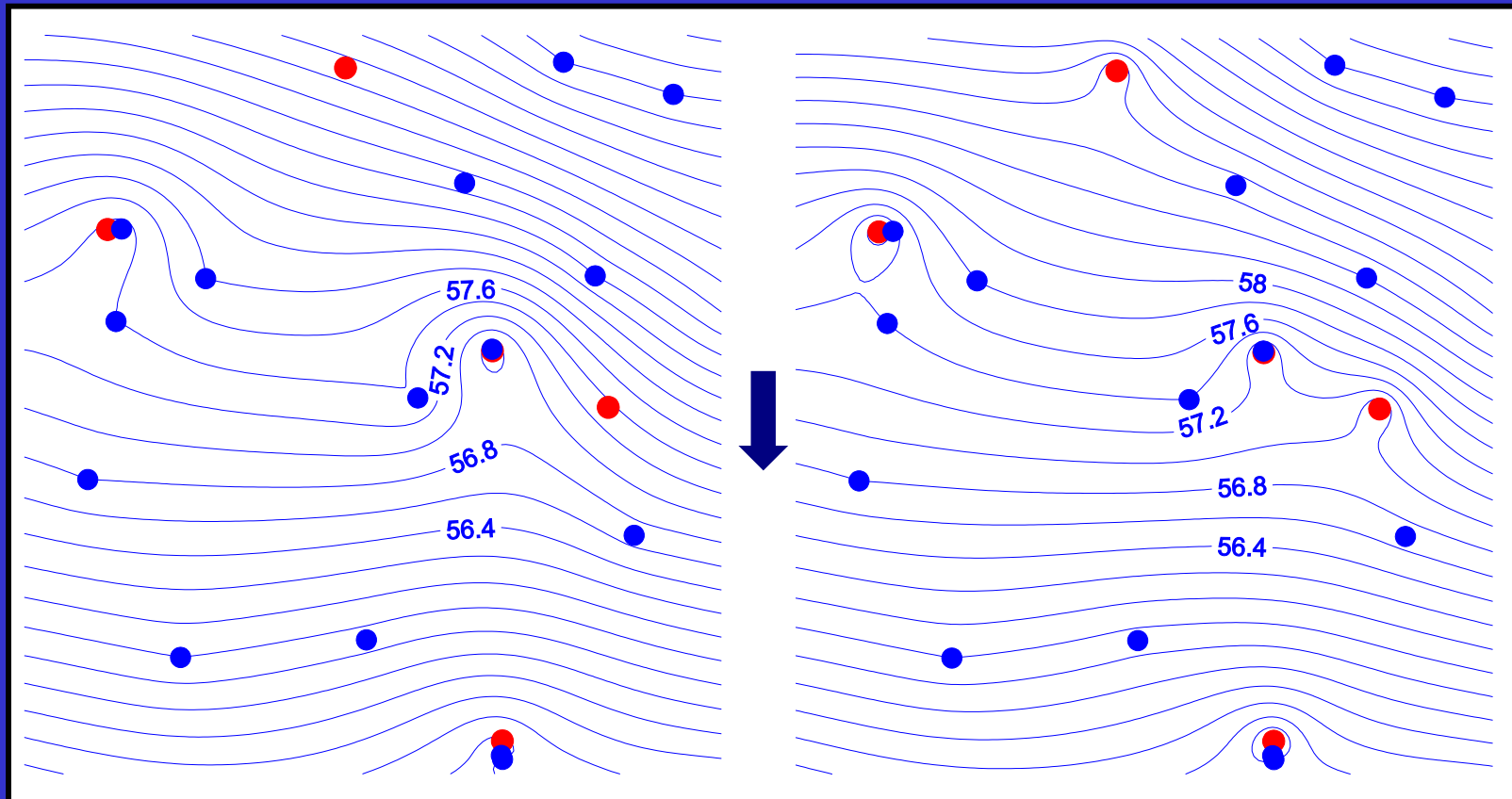
$$Z_{\text{est}} = f(Q, X, Y, R)$$



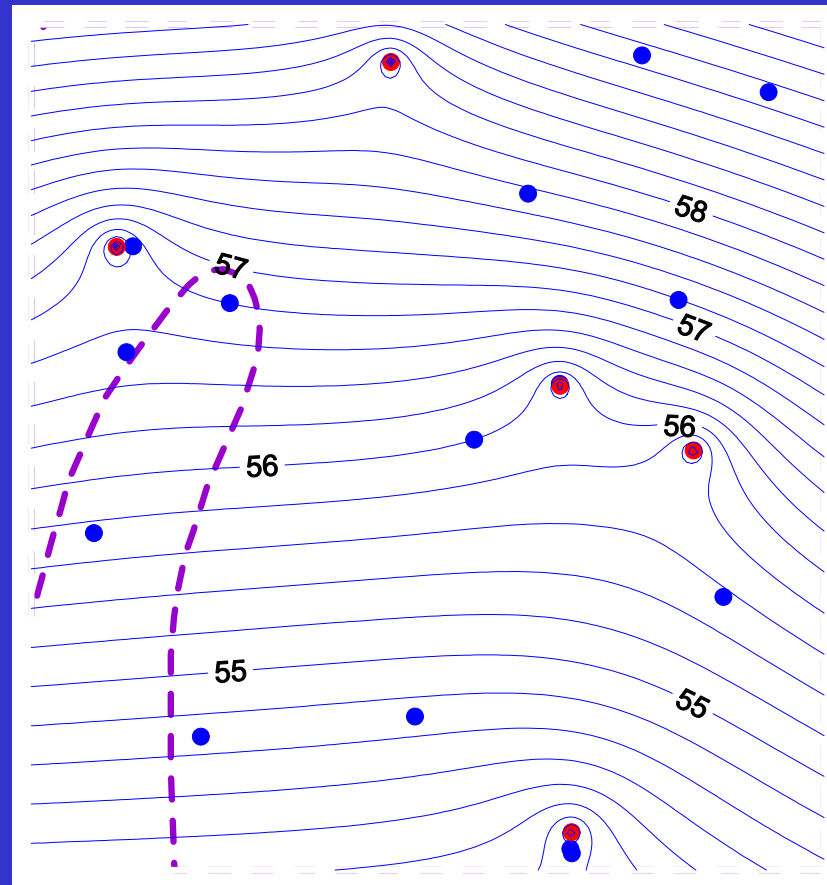
# Cape Cod - Comparison

Linear drift

Linear-log drift



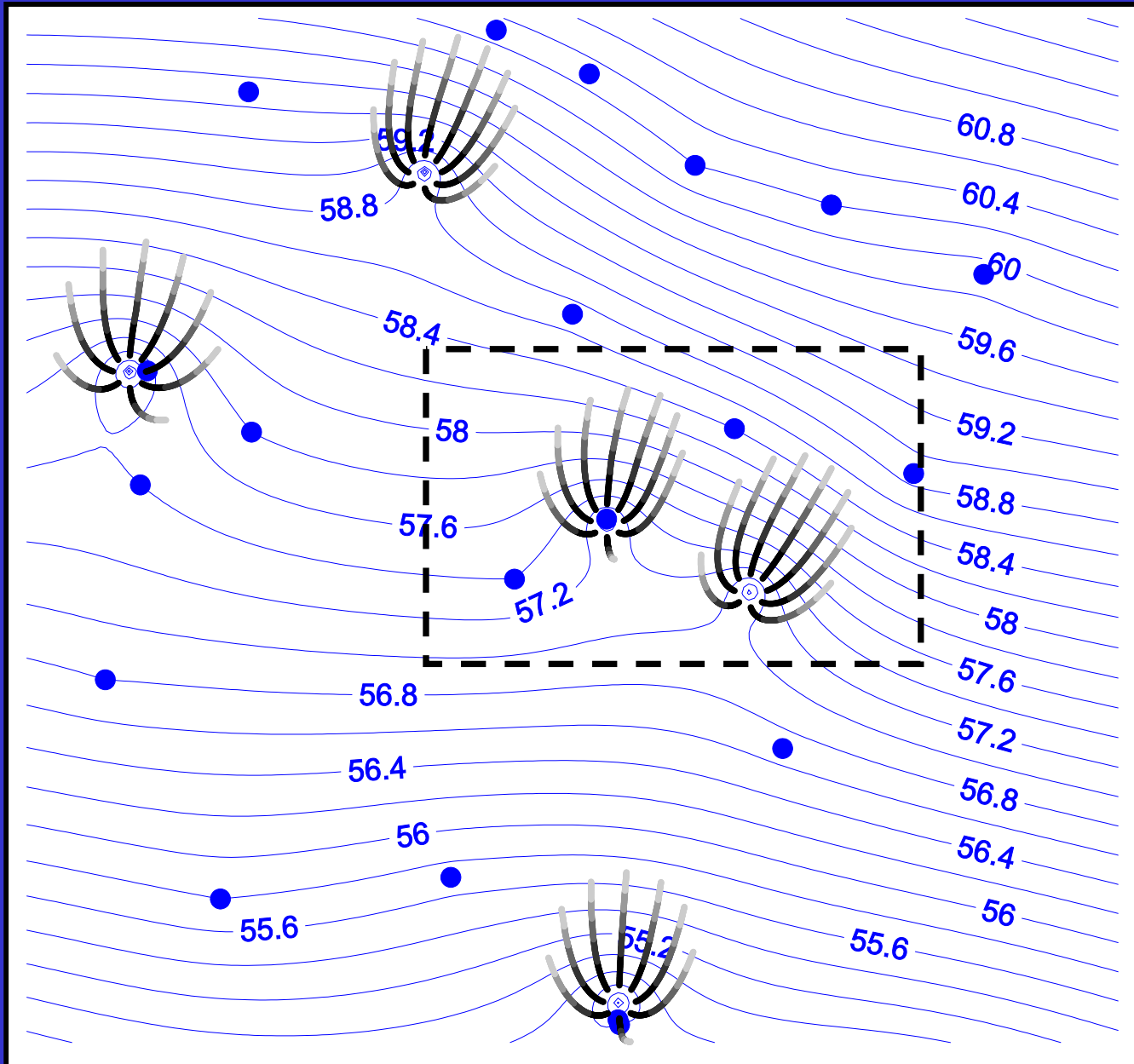
# Cape Cod - Trend Pattern



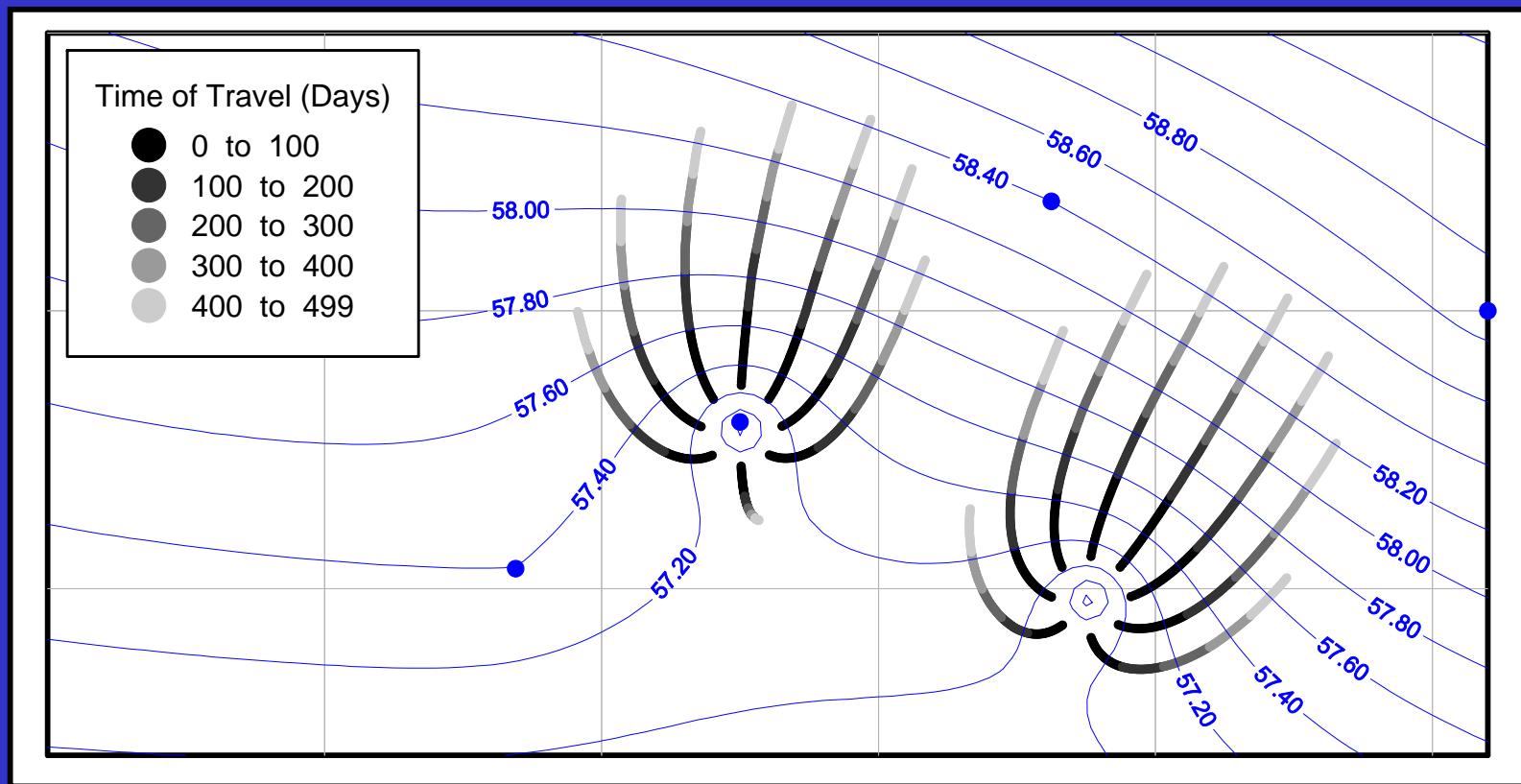
NOTE – estimated T was 56,000 ft<sup>2</sup>/d; from pump tests – 35,000 – 60,000 ft<sup>2</sup>/d



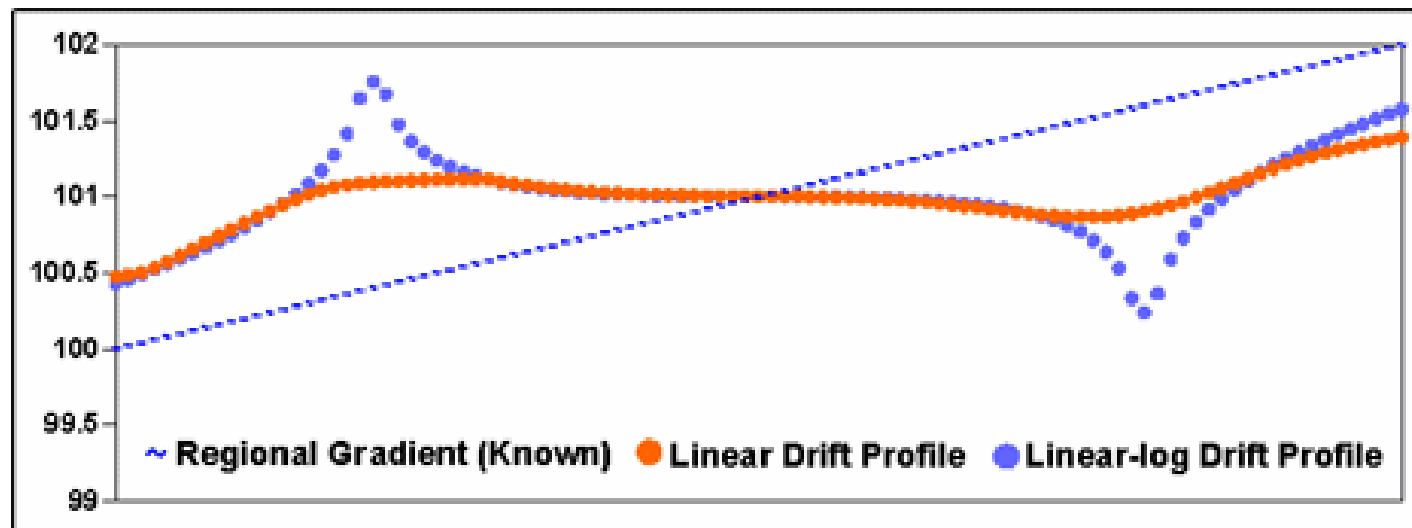
# Cape Cod



# Cape Cod

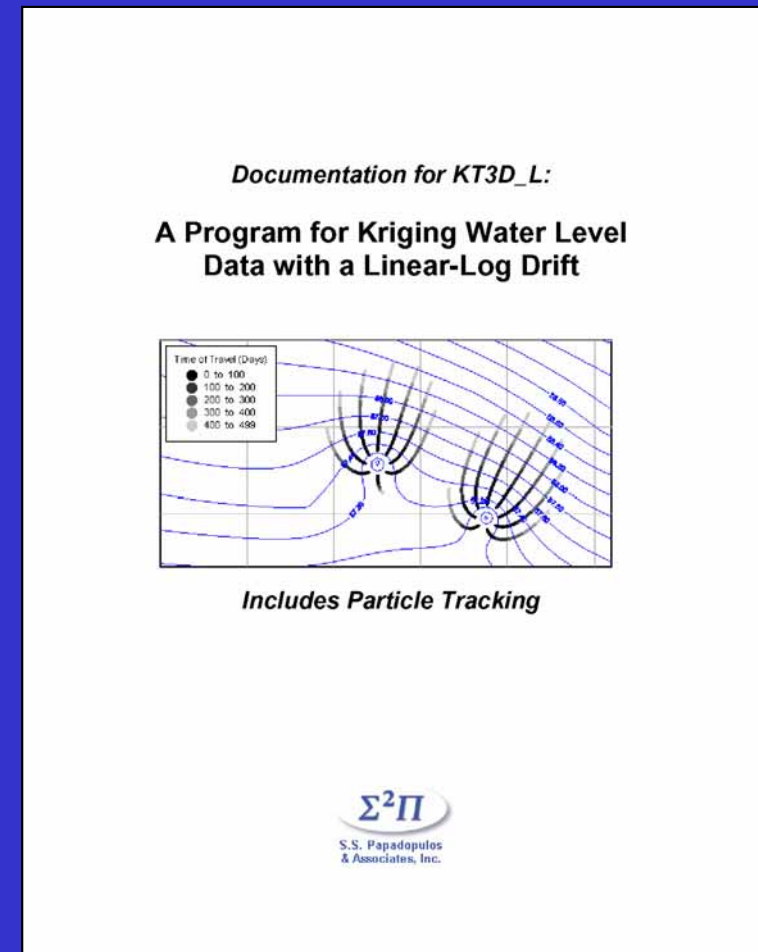
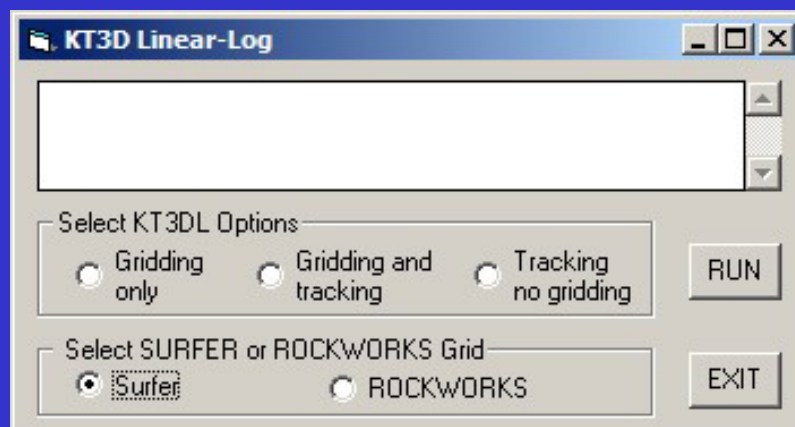


# Profile Example

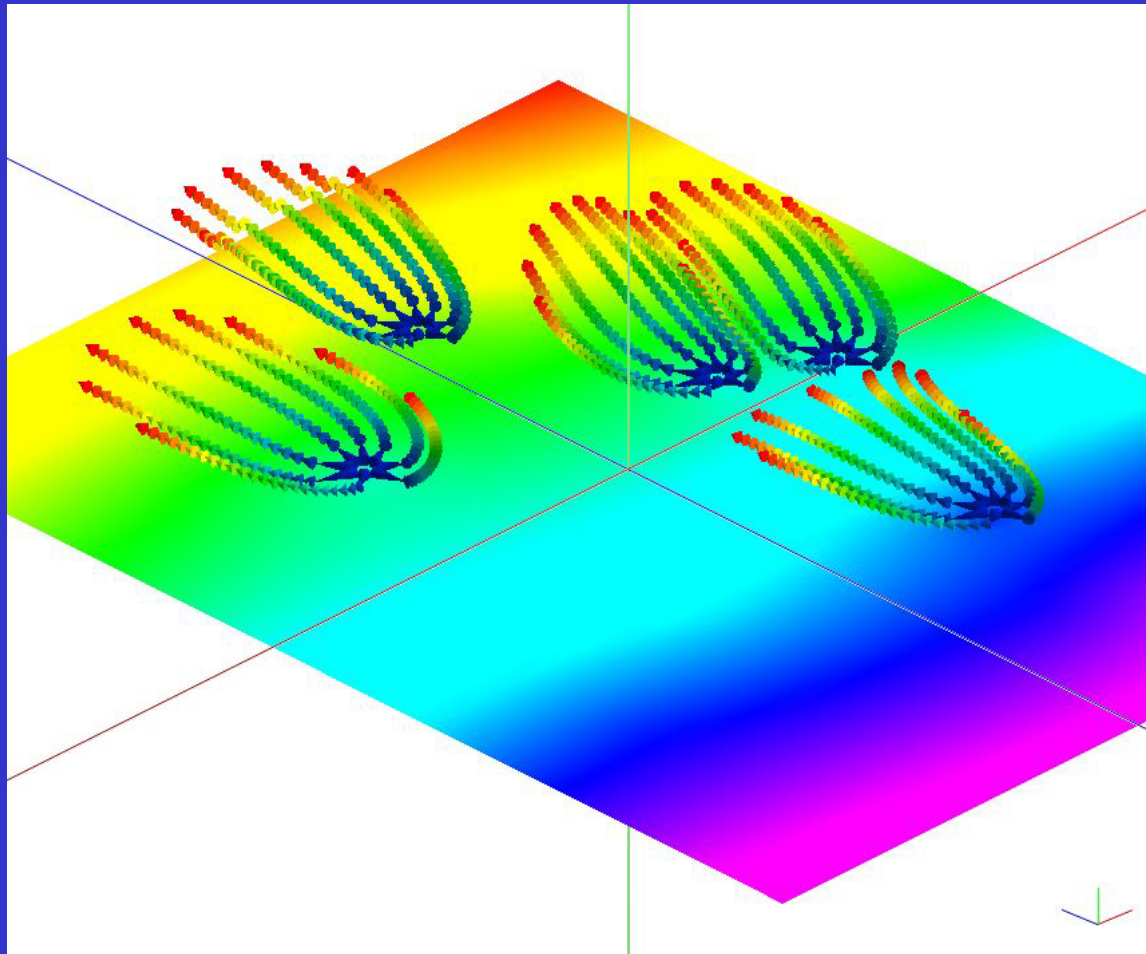


# Software

- Based on GSLIB program KT3D.
- GUI drives KT3D\_L1 including particle tracking.
- Surfer™ or Rockware™



# Rockworks



# Acknowledgements

- Air Force Center for Environmental Excellence (AFCEE)
  - In particular, Rose Forbes
- Jacobs Engineering Group
  - In particular, Mike Goydas, Dave Ward

